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This technical report has been reviewed and is approved for publication.

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data were fit to a seven-parameter equation in areal density at each sampling

altitude of the MORSAIR run. The fit coefficients for these data and plots of the $4\pi R^2$ silicon doses and the silicon K-factors, defined as the ratio of the two-dimensional real air $4\pi R^2$ dose to the mass integral scaled $4\pi R^2$ dose, are presented.

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PREFACE

i)

The author wishes to express his appreciation to Capt. Raymond A. Shulstad, the AFWL Project Officer, for his interest and assistance in the generation and evaluation of the data contained in this report, and to Eleanor Berthelot of Kaman Sciences for her assistance in making the MORSAIR runs, processing and fitting the results, and plotting the data.

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SECTION I INTLODUCTION

This report presents the results of fifteen computer runs made with the Kaman Sciences MORSAIR Monte Carlo computer program. These calculations were performed for the Air Force Weapons Laboratory (AFWL/SAT) under the direction of Capt. Raymond A. Shulstad.

The objective of this effort was to provide AFWL with a set of "real" two-dimensional atmospheric neutron and secondary gamma transport data for use in assessing the adequacy of mass scaled uniform air calculations. Previous studies at Kaman (ref. 1) and elsewhere (refs. 2, 3, 4) have indicated that large inaccuracies can result from scaling at high altitudes. The results presented in this report show the extent of these inaccuracies for two unclassified source spectra for both neutron and secondary gamma doses at al __tudes from 5 to 80 kilometers.

For each MORSAIR run, the neutron and secondary gamma doses in silicon and tissue as well as the total particle fluence were calculated using a Monte Carlo technique at more than 150 detector locations about a point isotropic source in the atmosphere. The spectra used in these runs were an unclassified fission source and an unclassified thermonuclear source, both of which were provided by AFWL (ref. 5). In addition to a run in homogeneous air with each source spectrum for the purposes of verifying the tracking and scoring techniques of the code, eight runs with the fission source and five with the thermonuclear source were made in the variable density atmosphere. Section II of this report describes in detail the energy bins, spectra, altitudes and dose response functions used in the calculations.

In section III the homogeneous atmosphere neutron and secondary gamma transport data supplied by AFWL and used in this study are described. The two homogeneous atmosphere MORSAIR runs made for checkout purposes are discussed. Also, in section III, the statistical uncertainties of the Monte Carlo data, the method used to fit these data, and the accuracy of these fits are briefly described. Finally, the method used to determine the K-factor, defined as the ratio of the $4\pi R^2$ dose in real variable density air to the $4\pi R^2$ dose in homogeneous air, is described.

In section IV, a brief discussion of some of the more obvious trends of the results is presented. The qualitative dependence of the K-factor on the source and detector altitude, mass range, source spectrum, and dose response function is described. The two primary effects which cause deviations from the scaled homogeneous air results, namely a leakage effect and a mass distribution effect are also described.

A summary of the calculations performed for this study and the conclusions which may be drawn from these results are presented in section V.

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In Appendix A, the tabulated fit coefficients of the one-dimensional ANISN $4\pi R^2$ dose data (used in defining the K-factors) are shown for the two source spectra. All of the $4\pi R^2$ doses have been plotted for both neutrons and secondary gammas and these are included in Appendix A. In Appendix B, the coefficients for the fits to the MORSAIR two-dimensional data are shown for each sampling altitude, dose response function, and particle type (neutron or secondary gamma). In Appendix C, plots of the fitted silicon dose data and the silicon K-factors for both neutrons and secondary gammas are shown for all 15 MORSAIR runs.

SECTION II CALCULATIONS

1. THE MORSAIR PROGRAM

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The Kaman Sciences MORSAIR program is an extensively modified version of the ORNL MORSE program (ref. 6) developed specifically for Monte Carlo calculations of radiation environments in a variable density atmosphere based on the 1962 Standard Atmosphere model (ref. 7). The multigroup cross section module of MORSE was used without modification, but the geometry and random walk modules were revised and a new scoring routine using an "extended path" or expectation boundary crossing estimator for scoring in concentric annular rings was added. In previous studies, the MORSAIR code has been used for calculating radiation environments at source altitudes from 20 to 65 kilometers. The results of those calculations have been checked against other Kaman real air transport codes, and codes from other agencies (ref. 8). It has been found to be a useful code for predicting radiation environments .t high altitudes where traditional methods of scaling uniform atmosphere results are inadequate.

The latest version of MORSAIR was written for use on the CDC 7600 computer and utilizes the fast access large core capability of that machine so that very large problems in terms of storage requirements can be efficiently handled by the code. In this study the time integrated neutron and secondary gamma doses and associated standard deviations were calculated for 58 energy groups at as many as 190 detectors spaced about the source. The differential energy spectra were recorded on magnetic tape so that doses other than those shown in this report can be calculated. Earth curvature effects were not included in the calculations, because these effects have been shown to be negligible at the altitudes and ranges of the calculations performed for this study (ref. 9).

2. INPUT PARAMETERS

The air cross sections used in the MORSAIR runs were the DLC-31 multigroup set distributed by the Radiation Shielding Information Center at ORNL (ref. 10). These cross sections were prepared from ENDF/B-IV data using a fission spectrum weighting function. A third order (P3) Legendre expansion was used to represent the angular variation of the cross sections. The nitrogen and oxygen cross sections were mixed to form the macroscopic cross sections of air with the following composition (ref. 5):

| Density: | l.ll mg/cm ³ |
|---------------------|---|
| Volume percentages: | 79 percent nitrogen 21 percent oxygen |
| Number densities: | 3.6609 x 10^{19} nitrogen atoms/cm ³ |
| | 9.7316 x 10^{18} oxygen atoms/cm ³ |

A copy of these cross sections was provided to Kaman by AFWL. The 37 neutron and 21 secondary gamma energy groups of the DLC-31 cross section set are shown in table 1. In table 2, the fraction of source neutrons in each of the groups is shown for the two unclassified spectra used in the calculations.

Three different response functions were used to weight the MORSAIR energy spectrum at each detector. Table 3 shows the neutron silicon and tissue dose response functions, and table 4 shows these response functions for the secondary gamma groups. The response functions shown in tables 3 and 4 were provided by AFWL (ref. 5). In addition to the silicon and tissue doses, the total number fluence was also calculated for both neutrons and secondary gammas.

DLC-31 ENERGY GROUP STRUCTURE

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| ĢPOUP | NEUTRON ENER | KGY (NEV) | GROUP | GAMMA ENERGY | (MEV) |
|-------|--|---------------|-------|--------------|------------|
| 1 | 1.9640E+01 - | - 1.6905E+01 | 38 | 1.40002+01 - | 1.0000E+01 |
| 2 | 1.6905E+01 · | - 1.4918E+01 | 39 | 1.0000E+01 - | 8.0000E+00 |
| 3 | 1.49188+01 - | - 1.41918+01 | 40 | 8.00002+00 - | 7.0000E+00 |
| 4 | 1.4191E+01 · | - 1.3840E+01 | 41 | 7.0000E+00 - | 6.0000E+00 |
| 5 | 1.38488+01 . | - 1+2840E+01 | 42 | 6.0000E+00 - | 5.0000E+00 |
| 6 | 1.2840E+01 · | - 1.?214E+01 | 43 | 5.0000E+00 - | 4.0000E+00 |
| 7 | 1.2214E+01 · | - 1.1052E+01 | 44 | 4.0000E+00 - | 3.0000E+00 |
| 8 | 1.10526+01 | - 1.0000E+01 | 45 | 3.0000E+00 - | 2.5000E+00 |
| 4 | 1.0000E+01 · | - 9.J484E+00 | 46 | 2.5000E+00 - | 2.0000E+00 |
| 10 | 9.04842+30 | - 8.1873E+00 | 47 | 2.0000E+00 - | 1.5000E+00 |
| 11 | 8.18732+00 - | - 7.4082E+00 | 48 | 1.3000E+00 - | 1.0000E+00 |
| 1? | 7.4082E+00 | - 6.3763E+00 | 49 | 1.0000E+00 - | 7.0009E-01 |
| 13 | 6.3763E+00 | - 4.9659E+00 | 50 | 7.0030E-01 - | 4.5000E-01 |
| 14 | 4.9554E+00 · | - 4.7237£+80 | 51 | 4.5000E-01 - | 3.0000E-01 |
| 15 | 4.7237E+00 | - 4.0657F+00 | 52 | 3.0000E-01 - | 1.5000E-01 |
| 16 | 4.0657E+00 | - 3.01196+0.0 | 53 | 1.50002-01 - | 1.0000E-01 |
| 17 | 3.0119E+00 | - 2.3852E+00 | 54 | 1.JOODE-01 - | 7.0000E-02 |
| 19 | 2.3852E+00 | - 2.3059E+00 | 55 | 7.0000E-02 - | 4.5000E-02 |
| 19 | 2.30692+00 | - 1.3263E+00 | 56 | 4.5000E-02 - | 3.0000E-02 |
| 20 | 1.8258E+00 | - 1.1080E+00 | 57 | 3.0000E-02 - | 2.0000E-02 |
| 21 | 1.1080E+00 | - 5.5023E-01 | 58 | 2.0000E-02 - | 1.0000E-02 |
| 22 | 5.50232-01 | - 1.5764E-01 | | | |
| 2.5 | 1.57648-91 | - 1.1109E-01 | | | |
| 24 | 1.1109E-01 | - 5.24/5E-02 | | | |
| 25 | 9+24/9E-J2 · | - 2.4/88E-92 | | | |
| 20 | 2+4/001-J2 · | - 2.15/5E-UZ | | | |
| 24 | 4 07775-02 | - 2 25.65-02 | | | |
| 20 | - 1 + U J J O E = U C · · - 7 - 75 / 4 ビー 0 2 | - 1 3740E-03 | | | |
| 2.3 | 3+37402-03 | - 6 423416-00 | | | |
| 30 | 5.82055-05 | - 4 04705-04 | | | |
| 32 | 1.01304-04 | - 101JUC-U4 | | | |
| 77 | 2.00238-04 | - 1.0677E=05 | | | |
| 34 | 1.06778-05 | - 3.05205-06 | | | |
| 35 | 3,05908-06 | - 1.1254E-06 | | | |
| 35 | 1.1254F-36 | - 4.14NAF-A7 | | | |
| 37 | 4.14905-07 | - 1.00008-11 | | | |
| | | *********** | | | |

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NEUTRON SOURCES

| GROUP | NEUTRON ENERGY (MEV) | THERMONUCLEAR | FISSION |
|-------|---|--------------------|--------------|
| 1 | 1.9640E+01 - 1.6905E+01 | 9 ÷ | 0. |
| 2 | 1.6905E+01 - 1.4918E+01 | 0. | 0. |
| 3 | Í•4918E+01 - 1•4191E+01 | 1.8870E-02 | 0. |
| 4 | 1.4191E+01 - 1.3840E+01 | 9.3400E-03 | 0. |
| 5 | 1.3840E+01 - 1.2840E+01 | 2.6620E-02 | 0. |
| ô | 1.2840E+01 - 1.2214E+01 | 1.6660E-02 | 0. |
| 7 | 1.22148+01 - 1.10528+01 | 1.6870E-32 | 0. |
| 5 | 1.10528+01 - 1.00008+01 | 1.2400E-02 | Û. |
| 9 | 1.0000E+01 - 9.0484E+00 | 7.4800E-03 | 3.8400E-03 |
| 10 | 9.0484E+00 - 3.1873E+00 | 6.82002-03 | 3.5000E-03 |
| 11 | 8.14738+00 - 7.40828+00 | 6.7800E-03 | 5.3900E-03 |
| 12 | 7.4032E+00 - 6.3763E+00 | 1.0300E-02 | 7.3500E-03 |
| 13 | 6.3763E+00 - 4.9659E+00 | 1.3070E-02 | 1.8370E-02 |
| 14 | 4:3659E+00 - 4.7237E+00 | 3.6200E-03 | 3.2500E-03 |
| 15 | 4•7237E+00 - 4•0657E+00 | 1.2430E-02 | 8.4700E-03 |
| 16 | 4.0657E+00 - 3.0119E+00 | 2.6040E-02 | 5.5000E-02 |
| 17 | 3.0119E+00 - 2.3852E+00 | 2.37302-02 | 3.2440E-02 |
| 18 | 2.38528+00 + 2.30698+00 | 3.75006-03 | 1.0580E-02 |
| 19 | 2.3069E+00 - 1.3268E+00 | 2.5640E-02 | 9.7240E-02 |
| 20 | 1.8268E+00 - 1.1080E+00 | 6.4450E-02 | 1.4677E-01 |
| 21 | 1.1080E+00 - 5.5023E-01 | 8.8490E-02 | 2.15672-01 |
| 22 | 5.5023E-01 - 1.5764E-01 | 9 .1380E-02 | 1.5018E-01 |
| 23 | 1.5764E-01 - 1.11095-01 | 1.1630E-02 | 1.9300E-02 |
| 24 | 1.1109E-01 - 5.2475E-02 | 1.1078E-01 | 1.2098E-01 |
| 25 | 5.2475E-02 - 2.4738E-02 | 5.4000E-02 | 5.7290E-02 |
| 26 | 2.4788E-32 - 2.1875E-02 | 5.6800E-03 | å.0000E-03 |
| 27 | 2.1875E-02 - 1.0333E-02 | 9.2640E-02 | 2.4000E-02 |
| 28 | $1 \cdot 0333E - 02 - 3 \cdot 3546E - 03$ | 1.1627E-01 | 1.4400E-02 |
| 29 | 3.3546E-03 - 1.2341E-03 | 7.3820E-02 | Ο. |
| 3Ú | 1.2341E-03 + 5.8294E-04 | 2.3240E-02 | 0. |
| 31 | 5.8294E-04 - 1.0130E-04 | 2.0280E-02 | 0. |
| 32 | 1.0130E-04 - 2.9023E-05 | 1.9000E-03 | θ. |
| 33 | 2.9023E-J5 - 1.0677E-D5 | 0. | 0. |
| 34 | 1.0077E-05 - 3.0530E-06 | 0. | 0. |
| 35 | 3.0590E-06 - 1.1254E-06 | 0. | ° 0 • |
| 36 | 1.1254E-06 - 4.14JOE-07 | 0. | 0. |
| 37 | 4.1400E-07 - 1.0000E-11 | 0. | 0. |

NEUTRON DOSE RESPONSE FUNCTIONS

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| GROUP | NEUTRON ENERGY | (MEV) | TISSUE DOSE | SILICON DOSE |
|-------|--------------------|-------------------|--------------|--------------|
| | | | RAD/ (N/C42) | RAD/(N/CM2) |
| 1 | 1.9648E+01 - 1.8 | 5905E+01 | 8.6724E-09 | 1.9106E-09 |
| 2 | 1.6905E+01 - 1.4 | 918E+01 | 7.4190E-09 | 1.7792E-09 |
| 3 | 1.49138+01 - 1.4 | 191E+01 | 6.8115E-09 | 1.6813E-09 |
| - | 1.4191E+01 - 1.3 | 8840E+01 | 6.5447E-09 | 1.6231E-09 |
| 5 | 1.3840E+01 - 1.2 | 2840E+01 | 6.14732-09 | 1.5144E-09 |
| 6 | 1.28478+01 - 1.2 | 214E+01 | 5.9548E-09 | 1.3851E-09 |
| 7 | 1.22146+01 - 1.1 | .052E+01 | 5.8936E-09 | 1.23706-09 |
| 8 | 1.1052E+31 - 1.0 | 1000E+01 | 5.5508E-09 | 1.0530E-09 |
| 9 | 1.0000E+J1 - 9.0 | 14346+00 | 5.2882E-09 | 8.7897E-10 |
| 10 | 9.0484E+90 - 8.1 | L873E+00 | 5.04732-09 | 7.9629E-10 |
| 11 | -8.1873E+00 - 7.4 | 092E+00 | 5.0045E-09 | 7.8141E-10 |
| 12 | 7.4082E+00 - 6.3 | 576 JE +0 0 | 4.7595E-09 | 4.7092E-10 |
| 13 | 6.3763E+00 - 4.4 | 1659E+00 | 4•4831E-09 | 2.1394E-10 |
| 14 | 4.9659E+JO - 4.7 | 237E+00 | 4.2531E-09 | 1.8267E-10 |
| 15 | 4.7237E+00 - +.0 | 1657E+00 | 4.1711E-03 | 1.4195E-10 |
| 10 | 4.0057E+30 - 3.0 | 113E+00 | 3.9784E-09 | 1.0582E-10 |
| 17 | 3.0119E+00 - 2.3 | 8922400 | 3.3905E-09 | 1.0006E-10 |
| 19 | 2.38522+00 - 2.3 | 8069E+0U | 3.1377E-99 | 8.2995E-11 |
| 19 | 2.3059E+30 - 1.8 | 3268E+00 | 3.0345E-09 | 9.4778E-11 |
| 20 | 1.82632+30 - 1.1 | L050E+00 | 2.6393E-09 | 6.5328E-11 |
| 21 | 1.1080E+00 - 5.5 | 5023E-01 | 2.0570E-09 | 4.9785E-11 |
| 22 | 5.50238-71 - 1.5 | 5764E - 01 | 1.3330E-09 | 3.1515E-11 |
| 23 | 1.57548-01 - 1.1 | 109E-01 | 7.62282-10 | 1.7897E-12 |
| 24 | 1.1109F-01 - 5.2 | 24752-02 | 5.48902-10 | 2.8022E-12 |
| 25 | 5.2475E-02 - 2.4 | +738E-02 | 3.1164E-10 | 1.2327E-12 |
| 26 | 2.4788E-02 - 2.1 | 18758-02 | 2.0739E-10 | 7.90848-13 |
| 27 | 2.1375E-02 - 1.1 | 13338-02 | 1.4662E-10 | 5.893DE-13 |
| 28 | 1.0333E-02 - 3.0 | 3546E-03 | 6.6143E-11 | 2.9804E-13 |
| 29 | 3.3546E-03 - 1.3 | 2341E-03 | 2.2758E-11 | 1.0498E-13 |
| 30 | 1.2341E-33 - 5.8 | 3294E-04 | 9.13152-12 | 4.3305E-14 |
| 31 | 5.8294E-04 - 1.0 | 130E-04 | 3.6632E-12 | 1.4421E-14 |
| 32 | 1.0133E = 04 = 2.5 | 9023E-05 | 1.1759E-12 | 4.5895E-15 |
| 3.5 | 2.9023E-05 - 1.0 | 1677E-05 | 1.10956-12 | 3.9377E-15 |
| 34 | 1.06772-05 - 3.0 | 1590E-06 | 1.6117E-12 | 5.6286E-15 |
| 35 | 3.0590E-06 - 1.1 | L254E-06 | 2.7416E-12 | 9+4023E-15 |
| 36 | 1.1254E-05 - 4.1 | L430E-07 | 4.4570E-12 | 1.5390E-14 |
| 37 | 4.1400E-07 - 1. |)000E-11 | 1.12385-11 | 7.42446-13 |

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GAMMA DUSE RESPONSE FUNCTIONS

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| GROUP | GAMMA ENERGY | (MEV) | TISSUE DOSE RAD/ (N/CM2) | SILICON DOSE |
|-------|--------------|-------------|-----------------------------|--------------|
| 1 | 1.4000E+01 - | 1.0000E+01 | 2.74318-09 | 3.4184E-09 |
| 2 | 1.0000E+01 - | 8.J000E+00 | 2.2564E-09 | 2.5712E-09 |
| 3 | 8.0000E+00 - | 7.0000E+00 | 1.9840E-09 | 2.1612E-09 |
| 4 | 7.0000E+00 - | 6.0000E+00 | 1.79222-09 | 1.8991E-09 |
| 5 | 6.0000E+00 - | 5.0000E+00 | 1.5928E-09 | 1.63672-09 |
| 6 | 5.0000E+00 - | 4.0000E+00 | 1.3897E-19 | 1.3835E-09 |
| 7 | 4.9000E+00 - | 3.30000+00 | 1.1803E-09 | 1.1335E-09 |
| 8 | 3.0000E+00 - | 2.50306+00 | 1.0098E-09 | 9.4334E-10 |
| 4 | 2.500%E+00 - | 2.00006+00 | d.9320E-10 | 8.2034E-10 |
| 10 | 2.00002+80 - | 1.30002+00 | 7.4281E-10 | 6.9343E-10 |
| 11 | 1.50008400 - | 1.00002+00 | 5.8030E-10 | 5.2846E-10 |
| 12 | 1.0000E+00 - | 7.9090Ě-01 | 4.2393E-10 | 3.8505E-10 |
| 13 | 7.0000E-01 - | 4.5000E-01 | 2.9695E-10 | 2.71228-10 |
| 14 | 4.5000E-01 - | 3.0000E-01 | 1.9283E-10 | 1.7772E-10 |
| 15 | 3.00005-01 - | 1.5000E-01 | 1.0770E-10 | 1.0459E-10 |
| 16 | 1.500VE-01 4 | 1.30306-01 | 4.9383E-11 | 6.8510E-11 |
| 17 | 1.0000E-01 - | 7.0000E-02 | 3.4315E-11 | 7.9854E-11 |
| 18 | 7.0009E-02 - | 4.5000E-02 | 2.9479E-11 | 1.4543E-10 |
| 19 | 4.50096-02 - | 3.000000-02 | 4.3750E-11 | 3.4411E-10 |
| 20 | 3.000.E-02 - | 2.10005-05 | J.6647E-11 | 8.2679E-10 |
| 21 | 2.0000E-02 - | 1.9000E-02 | 3.2504E-10 | 2.64938-09 |

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3. DESCRIPTION OF RUNS

A summary of the 15 MORSAIR runs made for this study is shown in table 5. In addition to the homogeneous atmosphere runs, eight runs were made using the fission source in real air at altitudes from 5 to 80 kilometers, and five thermonuclear source runs were made at altitudes from 20 to 80 kilometers. A minimum of 50,000 initial neutron histories were followed for each run, and the secondary gamma production rate was adjusted so that approximately the same number of gammas was produced in each run. For the lower altitude and homogeneous runs, the computer time required for 50,000 histories was greater than 30 minutes of CDC 7600 execution time. At the higher altitudes an appreciable number of the neutrons and secondary gammas escape out the "top" of the atmosphere after a few scatterings so that as many as 150,000 initial neutrons and approximately the same number of secondary gammas could be followed in less than 30 minutes.

A time cutoff of 20 seconds was used for each neutron history. This ensured that almost no neutrons were lost because of this cutoff.

The atmosphere model used in MORSAIR provides for a continuously varying density from sea level to 200 kilometers and very closely approximates the 1962 Standard Atmosphere model (ref. 7). Above 200 kilometers, a void is assumed and particles reaching this altitude are allowed to escape. The lateral extent of the atmosphere varied with each run to provide a large buffer beyond the last detectors of interest at each sampling altitude. This ensured that lateral leakage effects on the results would be negligible. Any particle reaching the ground (which only a very few did) was terminated.

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MORSAIR RUNS

| зег | Source | Source Altitude (km) | Number of Detectors | Neutron Histories | CDC 7600 Computer Time (Minutes) |
|-----|---------------|-------------------------|------------------------|----------------------|--|
| | Fission | Homogeneous | 190 | 50000 | 39 |
| | Fission | Ŋ | 165 | 50000 | 42 |
| | Fission | IO | 172 | 50000 | 36 |
| | Fission | 15 | 171 | 50000 | 33 |
| | Fission | 20 | 151 | 50000 | 31 |
| | Fission | 30 | ĩJ6 | 96000 | 30 |
| | Fission | 40 | 152 | 150000 | 30 |
| | Fission | 60 | 184 | 150000 | 20 |
| | Fission | 80 | 183 | 150000 | 21 |
| | Thermonuclear | Homogeneous | 190 | 50000 | 37 |
| | Thermonuclear | 20 | 151 | 50000 | 29 |
| | Thermonuclear | 30 | 156 | 93500 | 30 |
| | Thermonuclear | 40 | 152 | 150000 | 30 |
| | Thermonuclear | 60 | 184 | 150000 | 23 |
| | Thermonuclear | 80 | 1 83 | 150000 | 20 |

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Particle histories were terminated primarily because they escaped from the top of the atmosphere or their weight became so small that they could not contribute a significant score at any detector.

SECTION III RESULTS

1. HOMOGENEOUS ONE-DIMENSIONAL TRANSPORT DATA

The one-dimensional homogeneous air neutron and secondary gamma transport data used as a basis of comparison in this report were provided by AFWL (ref. 12). These data were generated by appropriate source spectrum weighting of Murphy's fits to Burgio's ANISN results (ref. 11). The resulting $4\pi R^2$ dose data were then fit to the equation:

 $\ln \left[4\pi R^{2} \text{ Dose}\right] = A + Bx + Cx^{2} + Dx^{3/2} + Ex^{1/2} + Fx^{1/3} + G \ln x$ for 0.1 < x < 300 gm/cm²

where x is the mass range of air or areal density in gm/cm². The seven coefficients representing the fits to the neutron and secondary gamma homogeneous atmosphere data are tabulated in Appendix A for the two spectra and three dose response functions used in this study.

For very small areal densities, between 0.0 and 0.1 gm/cm^2 of air which are of interest particularly at very high altitudes, a linear interpolation between the fitted ANISN $4\pi R^2$ dose at 0.1 gm/cm^2 and the uncollided $4\pi R^2$ dose (i.e., the sum over all energy groups of the products of the source fractions and dose response functions) at zero mass range was used to find the $4\pi R^2$ neutron doses. This method is commonly used in mass integral scaling codes to define atmospheric neutron environments at small mass ranges. A similar interpolation technique was used for the secondary gammas between zero and 0.1 gm/cm^2 of air, except in this case a $4\pi R^2$ dose value of zero was used at zero mass range.

*See footnote on page 35 for a definition of mass range.

The same energy groups, cross sections, sources, and dose response functions described earlier for the MORSAIR runs were used in the uniform air calculations.

2. MORSAIR VERIFICATION IN HOMOGENEOUS AIR

An option exists in the MORSAIR code to replace the variable density atmosphere model with a homogeneous atmosphere model. As an initial check on the scoring and tracking techniques employed in the code, one run for both the thermonuclear and the fission source spectrum was made using this option. It was anticipated that the results of such a run would agree with the one-dimensional ANISN infinite air results provided by AFWL from Burgio's calculations using the same spectra and response functions. Figures C-1 and C-3 of Appendix C show that for all sampling altitudes the difference between the fits of the ANISN homogeneous data and fits of the two-dimensional MORSAIR homogeneous data is less than 15 percent out to 100 gm/cm² and within 25 percent out to 200 gm/cm^2 for a fission source. Similar results for a thermonuclear source are shown in figures C-49 and C-51 of Appendix C. It should be emphasized that the solid lines shown in these and other figures of Appendix C represent the fitted one-dimensional homogeneous air ANISN d. 1, and the points are calculated from the fits of the MORSAIR data. It should also be pointed out that in the figures immediately following those mentioned above, namely figures C-2, C-4, C-50, and C-52 of Appendix C, the K-factors presented are actually ratios of fits of the homogeneous MORSAIR data to the ANISN data. All of the data in Appendix C is presented in this manner, i.e., the fitted homogeneous and real air data are shown first followed by the K-factors calculated from this data for each MORSAIR The differences between the ANISN and MORSAIR results run. for a homogeneous atmosphere are within the statistical

uncertainties of the MORSAIR data for these runs, and it was concluded that the MORSAIR tracking and scoring methods were correct.

3. STATISTICAL UNCERTAINTIES IN THE MORSAIR DATA

At the lowest source altitudes, the 50,000 neutron and secondary gamma histories resulted in standard deviations in the total doses of less than 15 percent out to 100 gm/cm^2 , and less than 25 percent to 200 gm/cm² in most cases. At source altitudes above 20 kilometers, the expectation boundary crossing scoring method is more efficient, and the statistical uncertainties in the data were somewhat less.

4. FITS TO THE MORSAIR DATA

To smooth the MORSAIR Monte Carlo results and to reduce the quantity of data to a more usable form consistent with the one-dimensional results, all of the $4\pi R^2$ doses were fit to the same seven parameter equation in areal density described above. For the MORSAIR data, it was found that dropping the last term, G ln x, did not affect the accuracy of the fits significantly and in some cases resulted in a slight improvement in the fit. For this reason, only six coefficients are used in the fits to the MORSAIR data shown in Appendix B.

The technique used to fit the data was a standard linear weighted least squares technique such as described in reference 13. The fitting method, it should be noted, was applied to the logarithm of the $4\pi R^2$ dose data where each data point was given a weight inversely proportional to the square of the logarithmic uncertainty in the MORSAIR data point. Any data point with a standard deviation greater than 50 percent was deleted before the fit was applied. The number of points removed for this reason was small for areal densities less than 200 gm/cm².

The fit coefficients for each run are tabulated in Appendix B. In addition, the range (in terms of minimum and maximum areal densities) over which the fit applies is shown. The last column in the tables, "RMS PCT DIFF", is the weighted root mean square percentage difference between the fit data and the actual MORSAIR data, i.e.,

"RMS PCT DIFF" =
$$\int \frac{\sum_{i} W_{i} Y_{i}^{2}}{\sum_{i} W_{i}} \times 100$$

where $Y_{i} = \ln \left[\frac{4\pi R^{2} \text{ actual MORSAIR dose}}{4\pi R^{2} \text{ fit MORSAIR dose}} \right]$

and the weight, W_i , was defined as:

| [| | | | | -2 |
|------------------|----|----|---|------------------|----|
| W _i = | ln | (1 | ÷ | σ _i) | |

where σ_i = fractional standard deviation of the MORSAIR dose.

As an example of the adequacy of the six parameter fit to represent the data, figure 1 shows both the actual MORSAIR data points and the values calculated from the fit for coaltitude neutron silicon doses from a thermonuclear source at 20 and 40 kilometers. Figure 2 shows the MORSAIR data points and the fit for the secondary gamma silicon dose. In general, it was found that this fitting technique resulted in a reasonably good representation of the actual data.

5. THE K-FACTOR

The adequacy of mass integral scaling of uniform air results to define real air environments can be conveniently described in terms of a K-factor which was first used by





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Figure 2. MORSAIR Data Points and the Fit to the Data Points for $4\pi R^2$ Secondary Gamma Silicon Dose, Coaltitude Sampling from 20 and 40 km Thermonuclear Sources

Marcum in his early high altitude transport studies (refs. 2, 3). The K-factor as used in this report is defined as

K-factor = $\frac{\frac{1}{2} \operatorname{The} 4\pi R^2 \operatorname{dose} \text{at a detector as calculated in a}}{\frac{1}{2} \operatorname{Teal}^2 \operatorname{variable density atmosphere} (\text{from fits to}}{\frac{\text{MORSAIR data in this case}}{1}}$

culated in homogeneous one-dimensional infinite air (from fits to the ANISN data in this case)

The K-factor, then, is a direct measure of the error associated with mass integral scaling of infinite air data due to the variable density nature of the atmosphere and can be used as multiplicative correction factor to the scaled data. A K-factor of 0.5, for example, indicates that in the real atmosphere the dose received is only one half of the dose that would be predicted by scaling methods.

Marcum's early studies and more recently those of Keith (ref. 1) and others (refs. 14, 15) have shown that the neutron K-factor is a function of source altitude, detector altitude, slant range, source energy, and the dose response function. The neutron K-factor, it has been shown, can vary from less than .1 at high source altitudes to greater than 5 for detectors below the source and at large areal densities. It is believed that while this study is more extensive in terms of the number of calculations performed and the range of altitudes and mass ranges covered, the data trends shown in this report for neutrons are in substantial agreement with the earlier data of Marcum and Keith. No previous attempts to calculate the transport of secondary gammas in a real atmosphere have been published.

Although there are many situations of practical interest in which the K-factor is near unity so that scaling results in small errors, there are also situations in which large
errors can result from neglecting variable density effects. It is hoped that the data presented in this report will allow a user to recognize those situations where scaling may be inaccurate.

In Appendix C, the $4\pi R^2$ silicon dose and the silicon Kfactor are plotted as a function of areal density for each of the MORSAIR runs. The trends of the silicon dose K-factors, as will be shown in section IV, are similar to those of the tissue dose and the total fluence K-factors so that in the interest of brevity, only the silicon dose and K-factor plots are shown.

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Definition of Mass Range (RHOR):
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In homogeneous air,

RHOR = $\rho(zs)R$

and in 2-D real air,

RHOR =
$$\int_0^R \rho(z) dR$$

where

 $\rho(z)$ = density as a function of altitude; $\rho(zs)$ = density at source altitude (zs); R = slant range between the source and a receiver point.

SECTION IV DISCUSSION

The K-factor, as defined previously, can be considered as a multiplicative correction factor to be applied to the scaled homogeneous air dose to account for the transport of neutrons and secondary gammas in the real variable density atmosphere. Since many computer codes used to predict neutron and secondary gamma environments in the atmosphere (such as ATR and SMAUG) use the method of mass integral scaling of homogeneous air transport data, it is believed that presenting the MORSAIR results in terms of K-factors allows a direct means of assessing the accuracy of these codes for source spectra similar to those used in this study.

The results of this study show that the K-factor is a complicated function of several parameters. In this section the dependence of the K-factor and therefore the validity of mass integral scaling of homogeneous air data on these parameters is described in a qualitative manner. A detailed explanation of the differences in the transport of neutrons and secondary gammas in homogeneous air and in a variable density atmosphere was beyond the scope of this effort.

1. K-FACTOR DEPENDENCE ON ALTITUDE AND MASS RANGE

In general as the source or detector altitude increases, more particles escape out the top of the atmosphere. Therefore, when compared to the mass integral scaled dose, the dose in a real atmosphere can be substantially less. This leakage effect has been demonstrated in many high altitude transport calculations. Figure 3 shows the coaltitude neutron K-factors for silicon at several source altitudes as calculated by MORSAIR for a fission source. For a detector at 40 gm/cm² from the source, the neutron K-factor is nearly unity for sources below



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20 kilometers, decreases to about 0.5 for a source at 30 kilometers, and is less than 0.2 for a 40 kilometer source altitude. The secondary gamma silicon K-factors exhibit a similar behavior as shown in figure 4, except the K-factors fall off even more at the higher source altitudes. Similar trends in the K-factors occur if the source altitude remains constant and the detector altitude changes as shown in figures C-27 and C-29 of Appendix C, for example.

In addition to this expected decrease with source and detector altitude due to leakage effects, it is also obvious from figures 3 and 4 that the K-factors are a strong function of the amount of air (areal density) between the source and detector. For detectors coaltitude with the source, the Kfactor at high altitudes decreases monotonically as the areal density increases, but at the 20 and ..0 kilometer source altitudes, the K-factor curve is more complicated.

Figure 3 shows that for these source altitudes, the neutron K-factor initially decreases with mass range as it does at higher altitudes due to leakage of particles from the atmosphere. At mass ranges of 80 to 100 gm/cm², however, the neutron K-factor begins to increase and at very large mass ranges it can be greater than 4 indicating that at these large ranges the actual dose can be more than four times the dose that is predicted by scaling the homogeneous transport This dose enhancement has been observed in earlier data. results (ref. 1), and is apparently due to the fact that a substantial number of the neutrons which arrive at these detectors at large mass ranges travel large distances in the lower density air above the detector and thus traverse less air than is predicted by the simple straight line mass integral between the source and the detector. They are therefore attenuated less than what would be predicted by the scaled



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homogeneous atmosphere results. This effect has been referred to as a "short circuiting" (ref. 15) or "mass distribution" (ref. 14) effect. While it is most apparent for detectors coaltitude and below the source at large mass ranges, this effect also occurs to a lesser extent for detectors above the source at large distances as is apparent from figure C-18, for example.

2. K-FACTOR DEPENDENCE ON DOSE RESPONSE FUNCTIONS

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The reduction or enhancement of the neutron dose in the real variable density atmosphere over the mass integral scaled dose depends not only on the source and detector altitudes as shown previously, but also on the dose response function used. For a source at 20 kilometers, it is shown in figure 5 that the neutron K-factors for the silicon and tissue doses and the total fluence are similar for sampling altitudes coaltitude with the source. At 40 kilometers, however, figure 5 shows that the neutron K-factors can be quite different, with the tissue dose K-factor being only half as large as the silicon K-factor, and the K-factor for fluence even smaller. These differences in the K-factors at high altitude are related to the fact that the response functions are different and the energy spectrum arriving at a detector in the real atmosphere can be quite different from the spectrum calculated in homogeneous air at the same areal density. From this example it is clear that the neutron real air effects depend strongly on the dose response function used to weight the neutron fluence.

While the secondary gamma K-factors are strong functions of source altitude and mass range from the source as shown in



figure 6, they are not so dependent on the response functions as was the case for neutrons.

3. K-FACTOR DEPENDENCE ON SOURCE SPECTRUM

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In figure 7 the coaltitude neutron silicon dose K-factor is shown for both the thermonuclear and fission source spectra at source altitudes of 20 and 40 kilometers. At 20 kilometers, the differences between the two K-factors are small at all areal densities, despite the fact that the two initial emitted spectra are quite different. At 40 kilometers, however, the silicon dose K-factors for the thermonuclear source are much larger than the K-factors for the fission source at areal densities less than 70 gm/cm^2 . At 40 gm/cm^2 , for example, the coaltitude neutron silicon K-factor for a thermonuclear source spectrum is twice as large as the Kfactor for a fission source. Similar results for the secondary gamma doses are shown in figure 8. At 60 gm/cm² the silicon K-factor for secondary gammas from a thermonuclear source is less than one-third of the silicon dose K-factor from a fission source spectrum coaltitude from a source at 40 kilometers. At 20 kilometers, however, the secondary gamma K-factors are nearly identical.

It is apparent from figures 7 and 8 that mass integral scaling can lead to very large errors in the neutron and secondary gamma environments in the atmosphere, and that the magnitude of these errors depends rather strongly on the source spectrum. In general, the K-factors for the fission source are less than those for a thermonuclear source indicating the scaling errors for this source spectrum are even greater than they are for a thermonuclear source.







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4. SECONDARY GAMMA K-FACTORS AT SMALL MASS RANGES

There is one feature of the results for secondary gamma doses at the highest altitudes, 60 kilometers and above, that deserves an additional comment. Figure C-84 in Appendix C is a good example of this data for the case of a thermonuclear source at 80 kilometers. The silicon K-factors for the higher sampling altitudes are very large at low mass ranges. The K-factor, as was pointed out in section 3, is the ratio of the $4\pi R^2$ dose in real air to the $4\pi R^2$ dose in homogeneous air. The homogeneous results for this study were based on ANISN code calculations. Because of the uncertainties in these results at small mass ranges, most scaling codes use an interpolation method between 0.0 and about 1.0 gm/cm². Such a method was used to produce the homogeneous data shown in Appendix A. No such approximations or assumptions were necessary in the MORSAIR results. So it should be noted that while the K-factors at these small mass ranges may not necessarily reflect differences between the homogeneous and real air results, they do reflect differences between the real air results and those from typical scaling codes.

SECTION V SUMMARY AND CONCLUSIONS

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In this report we have presented the results of 15 MORSAIR Monte Carlo code calculations of neutron and secondary gamma transport in a real variable density atmosphere. The two source spectra used in these calculations were an unclassified fission spectrum and an unclassified thermonuclear spectrum. The source altitudes varied from 5 to 80 kilometers and the energy dependent particle fluences were scored at more than 150 detectors located about the source for each run. The spectrum at each detector was weighted with fluence, silicon, and tissue dose response functions. The $4\pi R^2$ dose data has been fit to a seven parameter equation in areal density at each sampling altitude of the MORSAIR run. Coefficients of these fits and plots of the silicon dose and K-factors have been presented. We have shown how the K-factor, the correction to the scaled homogeneous transport data to account for variable density atmosphere effects, depends on several parameters.

As stated at the outset, the objective of this study was to provide data which would lend some insight into the accuracy of mass integral scaling of homogeneous air transport data at high altitudes. The data presented in this report demonstrate that mass integral scaling can lead to large errors particularly for source altitudes greater than 20 kilometers. We believe these data can serve as the basis of an algorithm for predicting the correction to the mass integral scaled dose for sources and response functions similar to those used in this study.

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APPENDIX A

ANISN HOMOGENEOUS AIR DATA

This appendix contains the coefficients of the fits to the neutron and secondary gamma transport ANISN code results provided by AFWL (ref. 12). The data was fit to the equation

 $\ln (4\pi R^2 \text{ Dose}) = A + Bx + Cx^2 + Dx^{3/2} + Ex^{1/2} + Fx^{1/3} + G \ln x$ where x is the mass range in gm/cm².

The coefficients of this fit for the different doses and sources are shown in Table 6.

The $4\pi R^2$ doses and fluences as calculated using these fits for both neutrons and secondary gammas have been plotted for the two source spectra in figures A-1 through A-6.

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Figure A-3. Homogeneous ANISN Fit Data. $4\pi R^2$ Neutron Fluence for a Fission and Thermonuclear Source.







Figure A-5. Homogeneous ANISN Fit Data. $4\pi R^2$ Secondary Gamma Tissue Dose for a Fission and Thermonuclear Source.



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APPENDIX B

FITS OF MORSAIR REAL AIR DATA

This appendix contains the results of a weighted least squares fit to the MORSAIR data. For each of the 15 MORSAIR runs, the following data is given at each sampling altitude:

- 1. The sampling altitude in kilometers.
- 2. The dose response function.

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 The minimum and maximum mass ranges at which the fit is considered valid. ŝ

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- 4. The coefficients to the fit equation:
- In $(4\pi R^2 \text{ Dose}) = A + Bx + Cx^2 + Dx^{3/2} + Ex^{1/2} + Fx^{1/3} + G \ln x$ where x is the mass range in gm/cm²
 - 5. The root mean square percentage difference between the fit values and the actual MORSAIR data.

These data are shown for both the neutron and secondary gammas.

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 3 FISSION SOURCE IN REAL AIR AT 10 km

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| | 5000 | PCT PCT DIFF | .973 | 677. | | .387 | • 400 | ì | 040. | • 416 | ; | + 110 • | + 62 • | c i | • • • • | 174. | | • 698 | .738 | | | | RHS | PCT DIFF | 205. | .354 | | .450 | .461 | 1 | .684 | . 70.8 | | 225 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | • 12 | 532 | | 306. | 372 | .367 | | |
|--|----------|-----------------------|---------|---------------|--------------|---------------|---------------|----------------|--|-----------------|---------------|---------------|------------------|---|---------------|----------------|--------------|---------------|--|-------------------------|---------------|--------------|--------------|-----------------------------------|------|---------------|--------------|---------------|---------------|--------------|---------------|-----------------------------|--------------|-------------------------------|---|---------------|---------------|---------------|--------------|---------------|---------------|--------------|---------------|
| | | IJ | 0. | 0. | 0. | 0. | •0• | 0. | .0 | • | •0• | .0 | • | •0• | • | • | ••• | .0 | •0• | 0. | | | | G | c | | | | | • | | • | • | • | •••• | • | ••• | •••• | ••• | •••• | • = c | • • | • 3 |
| | | le, | - | ••• | | •0 | 0. | 0. | •0 | • | •0 | 0. | • | • | 0. | • | •0• | •0 | •0 | •0 | | | | L. | c | • | | • | • | • | • | • | • | • | • | • • | •• | • | • | ••• | • | • | • • |
| 4 - | | Ŀ | | | | _ | | | | | | | | | | | | | | | | | | ш | | • | • | | • | • | • | | • | • | • | • | • | | • | • | • | • | • |
| SAIR RUN NO. AIR AT 15 kn | | COEFFICIENTS D | | | | | 0. | 0. | 75145E-02 0. | 11229E-01 0. | 19134E-01 0. | 46892E-02 0. | 36281E-02 D. | 76602E-02 0. | 0. | .0 | 0. | .0 | 0, | ••• | | | COEFFICIENTS | 0 | • | • • | •0 | ••• | • • • • | • | | -•28264E-U1 U | 27013E-01 U | 30275E-01 U | 14380E-01 0 | -•14049E-01 0 | 15219E-01 0 | .0 | 0 . | 0.00 | | •0• | |
| NTS FOR MORS CE IN REAL 2 | | FIT C | | • | • | 694905-04 | 53894E-04 | 68838E-05 | •22939E-03 | -39036E-03 | •63646E-03 | •11903E-03 | .87352E-04 | .22723E-03 | .45332E-04 | .40961E-04 | -37641E-04 | 50051E-04 | - 628255-05 | •50287E-04 | | | 113 | 3 | | •0• | •• | 0. | 120 69E-04 | 11770E-04 | 36536E-U4 | •94880E-03 | •89618E-03 | 10133E-02 | •43394E-03 | .42035E-03 | .46428E-03 | .31248E-04 | •44346E-04 | •42684E-05 | .10080E-04 | •14874E-U4 | 81247E-U5 |
| COEFFICIEI SSION SOUR | | ß | | 32504E-U1 | 30578F-01 | 22854E-01 | 26164E-01 | 34443E-01 | -29445E-01 | -53002E-01 | .11990E+00 | .96069E-02 | .718146-03 | .34928E-01 | 46112E-01 | | - 39833F-01 | 19635F-01 | - 30502E-01 | 42369E-01 | | | | 8 | | 21256E-01 | 21397E-01 | 20006E-01 | 17650E-01 | 18271E-01 | 82566E-02 | 20949E+00 | 20060E+00 | .22972E+00 | 10860E+00 | .10592E+00 | .11868E+00 | 27679E-01 | 30976E-01 | 19059E-01 | 18025E-01 | 19541E-01 | 13446E-01 |
| T T T T T T T T T | | ٩ | | 22760E+02 | 2003746107 | 22720E+02 | 187715+02 | 323005401 | 23283E+02 | 197855+02 | -52993E+00 | 22994F+02 | 19110E+02 | -17189E+01 | 215046402 | 178956+02 | 3 260 1 6401 | - 233165402 | | 109025702 .31513F+01 | | | | A | | 22019E+02 | 22166E+02 | 48282E+00 | 22267E+02 | 22346E+02 | 13552E+01 | 26104E+02 | 26084E+02 | 52489E+01 | 24667E+02 | 24716E+02 | 36914E+01 | 21460E+02 | 21381E+02 | 64818E+00 | 22343E+02 | 22341E+02 | 12412E+01 |
| | | MAX RHOR CHURNO | 202,009 | 195.600 | 195.000 | 196-000 | 100° • 101 | 001.744 | 194.000 | 108.000 | 190.300 | 186.900 | 194.700 | 194.700 | 106.700 | 195.700 | | | | 195.000 | | | | RHOR RHOR | | 195.600 | 195.600 | 195.600 | 194.900 | 194.900 | 194.900 | 198.000 | 198.000 | 198.000 | 194.700 | 194.700 | 194.700 | 195.700 | 195.700 | 195.700 | 195.000 | 195.000 | 195.000 |
| | | MIN RHOR | 202109 | 105.100 | 001.201 | 100.100 | | | 201-201-201-201-201-201-201-201-201-201- | 202.2 | 0.650 | 25.050 | 20.000 25.050 | 35,050 | | 76.000 | | 090 90 | | 96.960 06.060 | 006.06 | MMAS | | RHOR RHOR | | 105.100 | 105.100 | 105.100 | 58.450 | 58.450 | 58.450 | 3.793 | 3.793 | 9.650 | 35.050 | 35.050 | 35.050 | 76.900 | 76.900 | 76.900 | 96.960 | 96•960 | 96-960 |
| | NEUTRONS | SAMPLING ALTITUDE | | 11.30 SILICON | 11.30 TISSUE | 11.30 FLUENCE | 12.80 SILIGUN | 12.00 FI U0.51 | 12.00 FLUENCE | 10.4C3 SILICOUE | 17.424 11330C | 10427 FLOENCL | 17.03/ 31L2000 | 4 4 4 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 11.00 TLUCACE | O 21 66 TICSUE | | ZI.66 FLUENCE | 20.01 SILLUN | 25.51 TISSUE | CD+DI LLUCHUC | SECONDARY GA | | SAMPLING ALTITUDE //w/ DASE | | 11.30 SILICON | 11.30 TISSUE | 11.30 FLUENCE | 12.80 SILICON | 12.80 TISSUE | 12.80 FLUENCE | 25.29 SILICON | 15.29 TISSUE | 15.29 FLUENCE | 17.37 SILICON | 17.37 TISSUE | 17.37 FLUENCE | 21.66 SILICON | 21.66 TISSUE | 21.66 FLUENCE | 25.51 SILICON | 25.51 TISSUE | 25.51 FLUENCE |

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FIT COEFFICIENTS FOR MORSAIR RUN NO.

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ഹ FIT COEFFICIENTS FOR MORSAIR RUN NO. FISSION SOURCE IN REAL AIR AT 20 km

| | RMS PCI UIFF | 2.151 2.288 | 617 | 164. | | .224 | • 364 | 0 | • 316 | 007. | 020 | 0000 | C J J • | 7 4 C | 7.75 | | | | RHS | DIFF | .386 | - 376 | | .357 | . 358 | | .561 | • 560 | | • 398 | .402 | | .255 | .267 | | | 477. | |
|----------|------------------------------|------------------------|--------------|--------------|---------------------------------------|--------------|-------------|--------------|--------------|-------------------------------|-----------------|--------------|-------------|--------------|--------------|-------------|--------------|--------------|------------|--------------------|------|--------------|-------------|--------------|--------------|---------------------|--------------|--|----------------|--------------|-------------|---------------|--------------|-------------|--------------|--------------|-------------|--------------|
| | ى | с. О. | •0 | • • | •0 | .0 | •0 | | • | • • | ••• | • | • | • | • | • | • • | | , | U | | | • | | | | •0 | .0 | 0. | 0. | •0 | . | •0 | • 0 | • | • | • | |
| | L. | ••• | •0• | • | | ••• | 0. | • | • | .0. | • | • | • | • = 0 | • • | • | | | | L. | c | • | • | | | | • 0 | 0. | • 0 | 0. | 0. | •0 | 0. | 0. | • | • | ••• | • 0 |
| | ຟ | | | | | | | | | | | | | | | | | | | ษ | | | | | | | | | | | | | | | | | | |
| | IS | | | • | | | • | • | • | • | • | •• | •• | • | • | | | | TS | | c | | • • | | | | | .0 | • | • | • | • | • | • | • | • | • | • |
| | r coefficien 0 | ••• | • 0 | . | • | 83187E-02 | 93537E-02 | 19665E-01 | 62228E-02 | 67195E-02 | 13146E-01 | 16530E-02 | .14918E-02 | 33789E-02 | .52512E-02 | •74050E-02 | .90739E-02 | | COEFFICIEN | 0 | c | ••• | * 0 | • | • | • | 30242F-01 | 29642E-01 | 32353E-01 | 23641E-01 | 23440E-01 | 23537E-01 | 79982E-02 | 74484E-02 | 12665E-01 | .11284E-02 | •16304E-02 | •21684E-UZ |
| | C FII | • • • | .0 | 174425-04 | • • • • • • • • • • • • • • • • • • • | .296465-03 | .32934E-U3 | .725716-03 | .24718E-03 | 26595E-U3 | • 4 96 85 E- 03 | •14199E-03 | •40365E-05 | •18282E-03 | 751366-04 | 172736-03 | 24472E-03 | | FI | U | | •••• | • | | | - 276 AV 576 - 44 - | | -10112F-02 | .112756-02 | .82754E-03 | .82225E-03 | .80759E-03 | .23942E-03 | .21777E-03 | .41287E-03 | 10206E-03 | 12262E-03 | 10426E-03 |
| | 3 | 35872E-01 44564E-01 | 31650E-01 | 29758E-01 | | -31543F-01 | .414726-01 | 11808E+00 | .12286E-01 | •17341E-01 | .69653E-01 | 32571E-01 | 50332E-01 | 94284E-02 | 94457E-01 | 10540E+00 | 11109E+00 | | | ß | | | 27217E-01 | 10-3195000+ | - TO/DZE+UT | | | .217815+00 | 234655+00 | .16984E+DO | .16749E+00 | .17462E+00 | .55748E-01 | .51479E-01 | .91537E-01 | 13687E-01 | 17037E-01 | 27887E-01 |
| | A | 22335E+02 17028E+02 | .20633E+01 | 22626E+02 | 1861UE+UZ | 2334F+02 | 19776E+02 | .48472E+00 | 23020E+02 | 19383E+02 | .11283E+01 | 22202E+02 | 18344E+02 | 22669E+01 | 21063E+02 | 17345E+02 | .36959E+01 | | | ٩ | | Z1067±+UZ | 21659E+02 | •92595E+UU | 2259/E+UZ | 220555442 | - JELYJETUL | | 54619F+01 | 26671F+02 | 257055+02 | 46048E+01 | 24075E+02 | ~.24086E+02 | 33905E+01 | 23002E+02 | 23031E+02 | 14404E+01 |
| | HAX RHOR GH/CH2 | 195.400 195.400 | 195.400 | 200.000 | 185.700 | 102.501 | 193,900 | 193.500 | 180.000 | 180.000 | 180.000 | 197.500 | 197.500 | 197.500 | 196.800 | 196.600 | 196.300 | | MAX | RHOR GM/CM2 | | 195.400 | 195.400 | 195.400 | 200.000 | 200.000 | 200.000 | 000 TOT | 102-000 | 195.400 | 195.400 | 195.400 | 197.500 | 197.500 | 197.500 | 196.400 | 196.800 | 195.80U |
| | MIN RHOR GM/CM2 | 146.500 146.500 | 146.500 | 022.27 | 022-22 | | 671•7 | 10.690 | 13.370 | 13.370 | 19.220 | 32-110 | 32.110 | 32.110 | 47.910 | 47.910 | 47.910 | MHAS | NIN | RHOR GM/CM2 | | 146.500 | 146.500 | 146.500 | 022-22 | 0/1.77 | | 5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | | 1 2 2 2 1 | | 19.220 | 32.110 | 32.110 | 32.110 | 47.910 | 47.910 | 47.910 |
| NEJTRONS | KPLING TITUDE Km) Dosē | 2.10 SILICON | 2.10 FLUENCE | 4.85 SILICON | 4.85 TISSUE | 4.85 FLUENCE | 0.61 TISSUE | 0.61 FLUENCE | Z-DB SILICON | 2.08 TISSUE | 2.08 FLUENCE | o.13 SILICON | 6.13 TISSUE | 6.13 FLUENCE | 4.72 SILICON | 4.72 TISSUE | 4.72 FLUENCE | SECONDARY GA | NPI ING | TITUDE KHJ DOSE | | 2.10 SILICON | 2.10 TISSUE | 2.10 FLUENCE | 4.85 SILICON | 4.85 TISSUE | 4.85 FLUENCE | NOT STRUCK | 0 64 51 113305 | D DY STITCON | 2 DA TISSUE | 2.08 FI HENCE | 6.13 SILICON | 6.13 TISSUE | 6.13 FLUENCE | 4.72 SILICON | 4.72 TISSUE | 4.72 FLUENCE |
| | SA AL | | | - | ٦ | | 5 0 | 1 (| i N | | | N I | 2 | 2 | (") | M | (11) | | 20 | AL AL | • | - | - | -1 | - | - | H (| v (| v | u r | 4 0 | 1 / | 3 (1) | 1 (1) | , N | 1.173 | (1) | ·~) |

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Å 0 N 30 RUN FISSION SOURCE IN REAL AIR AT MORSAIR FOR FIT COEFFICIENTS

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| SAMPLING Altitude (KM) duse | HIN RHOR GH/CH2 | MAX RHOR GM/ LH2 | ط | B | L J | r cuefficient D | υ | u. | 3 | RM PC | 2 H H |
|--|--|--|---|--------------------------------------|--|--|--------------------------------|------|-----|--------------|----------|
| 15.00 SILICON 15.00 TISSUE | 114.200 114.200 | 192.500 192.500 | 21952£+02 18446£+02 | 39714E-01 37586E-01 | ••• | | ••• | ••• | ••• | 1.01 1.03 | ي و ب |
| 15.00 FLUENCE 20.00 SILICON 20.00 TISSUF | 114.200 46.240 46.240 | 192.5J0 180.000 180.000 | .2358354UI 222555E+D2 18067E+02 | 58453E-01 58453E-01 83583E-01 | | .33264E-02 .64447E-02 | | | | . 30 | d ک |
| 20.00 FLUENCE 30.00 STLICON | 46.240 1.755 | 180.000 200.000 | .298896+01 242736+02 | 66274E-01 18263E+00 | 11467E-03 73759E-04 | .44273E-02 .86540E-02 .13892F-01 | 0. .83658E+00 .10550E+01 | | ••• | 46° | νs |
| 30.00 TISSUE 30.00 FLUENCE 40.00 SILICON | 1.755 2.200 1.040 | 200-000 200-000 170-400 | +.21014E+U2 13815E+01 22805E+02 | 231685700 273686400 174746-01 | 41796E-03 .33951E-03 | | •14633E+01 0. | | ••• | • 28 | 40 |
| 40.00 TISSUE 40.00 FLUENCE 50.00 SILICON | 11.040 14.550 13.200 | 170.400 170.400 80.000 | 19151E+U2 .12441E+01 22404E+02 | 191395-U1 .667715-U2 736395-U1 | | | | | ••• | .22 | 55 |
| 50.00 TISSUE 50.00 FLUENCE 60.03 SILICON 60.00 TISSUE | 13.200 13.200 13.800 13.800 13.800 13.800 | 80°000 80°000 119°000 119°000 | 100945+42 .201025+01 222205+02 187505+02 .205575+01 | | 11662E-03 11662E-03 .34040E-04 .31344Ê-04 | •58309E-02 •47552E-02 •88411E-03 •49940E-02 | | | | . 22 | 55 |
| SECONDARY GA Sampling Altitude | HHAS HIN Rhor | tiax Rhor | ٩ | ۵ | L FI | T COEFFICIENT D | ω N | لد. | ى | AR PC | ST F |

.15106-03 .151826-03 .2549766-03 .264766-03 .104196-03 .172616-03 .516976-03 .516976-03 .518076-03 .518076-03 .518076-03 .518076-03 .518076-03 .518076-03 .518076-03 .519566-03 .416046-030 -.23418E-01 -.24261E-01 -.18617E-01 .12850E-01 .12850E-01 .45352E-01 .45352E-01 .45352E-01 .45352E-01 -.31832E+00 -.31832E+00 -.31145E+00 .86716E-01 .86716E-01 .86716E-01 .86716E-01 .11145E+00 .86716E-01 .26836E-01 .11145E+00 .1114 192.500 192.500 192.500 198.500 198.500 198.500 198.500 198.500 198.500 198.500 198.500 198.500 198.500 198.500 119.000 119.000 119.000 GM/CM2 GH/CH2 SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE SILICON TISSUE SILICON TISSUE SILICON TISSUE DOSE 202 Ĩ

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| | RHS PCT LIFF | • 458 | | .165 | 141. | .162 | .243 | | • 141 | anz • | (A) | .148 | | .037 | .053 | | | RHS | PCT | 1170 | .267 | .284 | : | 455° | . 333 | .338 | 1221 | | .363 | • 364 | 1 | • 222 | • 22 9 | 144 | 271 | • • • |
|-----------|-----------------------------------|--------------------------|---------------|---------------|----------------|------------------------|------------------------|---------------|---------------|--------------|---------------|---------------|--------------|----------------|---------------|----------------|--------------|--------------|----------|-----------|-------------------------------|-------------------------------|---------------|---------------------|--------------|---|---------------|------------------|---------------|-------------|-----------------------------|-------------------------------|--------------|---------------|----------------------|--------------------------|
| | و، | 0. | • 0 | | • | • • | | ů. | | • | | • | • 0 | • 0 | 0. | .0 | | | 9 | | 0. | | • | • | . | | | | | • | • | • | • | •••• | • | |
| | LL. | | | . . | | • • | | D. | 0. | 0. | | • | | • | Ú. | U. | | | ۱Ľ. | | ئ. ا | .0 | - | | д. | 0. 10.0575 ±0.0 | 15 2055 40 2 | .165875+01 | Ū. | Ũ. | •0 | . | ••• | | • | ••• |
| | ш is | • | • | • 0 | | 0. . 569895 4 NN | .81747E+00 | .12907E+01 | 0. | • • | | • • • | | • • | .0 | 0. | | | w | | G. | . | 0. | .0 | • | 0. _ 067075101 | | | 0. | 0. | . | .0 | | • • | •••• | ••• |
| | CUEFFICIENTS D | •0 | D. | 14985E-01 | 11245E-01 | 11643E-01 28:865-02 | .56954E-02 | .17118E-01 | 34911E-01 | 42967E-01 | 35842E-01 | 44120E-01 | 25U105-U1 | 42014E-01 | 515446-01 | 46881E-01 | | COEFFICIENTS | 0 | | 0. | 0. | 0. | 37945E-01 | 38040E-01 | 34645E-01 | | 11400UCTUU | 12357E+00 | 12357E+00 | 14330E+00 | 14674E+00 | 14909E+00 | 16492E+00 | | 159112+VU 150742+00 |
| | C FII | .82744E-04 .75636F-04 | •37861E-04 | •88112E-03 | • 6 93 60 E-03 | .642915-03 | .34600E-03 | 83743E-04 | .27931E-02 | •36063E-02 | -29530E-02 | .43998E-02 | 202575-02 | .429065-02 | .572852-02 | .65226E-02 | | FIT | ი | | 21866E-04 | 25265E-04 | .27114E-04 | .17652E- 3 2 | .17762E-02 | 15674E-02 74275-02 | | -124C0C-UC | -93974E~02 | .94016E-02 | 11449E-01 | .13739E-01 | .13961E-01 | .15816E-01 | •143005-01 •••••• | .14619E-U1 .14321E-U1 |
| | Ð | 45868E-01 45368E-01 | 31547E-01 | .27457E-01 | •93676E-02 | .23320E-01 | 20769F+00 | 31961E+00 | .52695E-01 | •65139E-01 | • 22355E-01 | •49839E-UI | - 500505-05 | | .41190E-01 | 20720E-01 | | | 8 | | 25431E-01 | 26393E-D1 | 24513E-01 | .19379E+00 | .19307E+00 | .18181E+00 | 101300011. | - 3759254AD | • 38984E+00 | • 39051E+00 | •42693E+00 | 36778E+00 | .37548E+00 | • 3994 0E+00 | • 2851 / E+UU | .2452UE+UU .24531E+90 |
| | z | 22360E+02 | -207136+01 | 23292E+02 | 19568E+02 | .10180E+01 | 23855EFUC 26569F+02 | 86160E+00 | 23164E+B2 | 15599E+02 | •86529E+00 | 23049E+02 | -*143/2E+UC | 77008F407 | 193916+02 | .11303E+01 | | | ٩ | | 22869E+02 | 229536+02 | 14491E+01 | 25957E+02 | 259996+02 | 46680E+01 | 224342700. | | 25987E+02 | 26013E+02 | 48575E+01 | 25552E+02 | 25594E+02 | 44712E+01 | 252046+66 | 25253£+UZ 39886E+01 |
| | MAX RHOR GM/ CN2 | 179.300 | 179.300 | 120.600 | 120.600 | .20.60U | 76.530 | 76.530 | 42.630 | 42.630 | 42,630 | 32,420 | 52.4CU | 26.46U | 24.550 | 24.550 | × | HAX | RHOR | GM/CH2 | 179.300 | 179.300 | 179.300 | 120.600 | 120.600 | 120.600 | 140 °21 | 12.650 | 42.630 | 42.630 | 42.630 | 32.420 | 32.420 | 32.420 | 24.550 | 24.550 24.550 |
| | MIN RHOR GM/CM2 | 54.830 | 54.830 | 10.110 | 10.110 | 11.610 | 047. | 5.209 | 3+45 | 3.445 | 4.985 | 3.661 | 100.0 | 2• 40U | 3-674 | 3.674 | HHAS | NIN | RHOR | GH/CH2 | 54.830 | 54.830 | 54.830 | 10.110 | 10.110 | 11.610 | na/• |) (/ ° 7 C O | 3.445 | 3.445 | 4.985 | 3.661 | 3.661 | 3.661 | 3.574 | 3•674 3•674 |
| NEILTONNS | SAMPLING ALTITUDE (KH) DOSE | 20.00 SILICON | 20.00 FLUENCE | 30.00 SILICON | 30.00 TISSUE | 30.00 FLUENCE | 40.00 SILICON | 40.00 FLUENCE | 60.00 SILICON | 60.00 TISSUE | 00.00 FLUENCE | 80.00 SILICON | 80.00 IISSUE | ADD DD STITCON | 100.00 TISSUE | 100.00 FLUENCE | SECONDARY GA | SAMPLING | ALTITUDE | (KH) DOSE | 20.00 SILICON | 20.00 TISSUE | 20.00 FLUENCE | 30.00 SILICON | 30.00 TISSUE | 30.00 FLUENCE | 40.00 STLICUN | 40.00 IISSUE | 66.00 STLICON | 0.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 80.00 TISSUE | 80.00 FLUENCE | 100.00 SILICUN | 100.00 TISSUE |

FIT COEFFICIENTS FOR MORSAIR RUN NO. 7 FISSION SOURCE IN REAL AIR AT 40 km

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| | 010 | PCT DIFF | . 65 d | 100. | | | 411. | 0.7.0 | 5. n · | n T T * | .034 | .026 | | .022 | .033 | | .030 | .036 | | | RHS | PCT DIFF | с Ч | - to t | | .260 | .196 | | .106 | .100 | COL | | | .108 | .104 | 1 | .108 | .167 | |
|-------------|----------|-----------------------------------|---------------|--------------|---------------|---------------|--------------|-------------------------------|---------------|--------------|------------------------|---------------------|----------------|------------|--|----------------|----------------|---------------|--------------------|--------------|--------------|-------------|---------|---------------|--------------|-------------------------|----------------|---------------|---------------|----------------------|---------------|-----------------|--------------|---------------|-------------------------|---------------------|-----------------------|-----------------|--|
| | | IJ | • • | | | ÷. | | | • | • - | • | | .0 | 0, | 0. | 0. | . | Û. | •• | | | ۍ | | | ••• | 0. | 0. | 0. | 0. | ••• | ••• | • | • • | | .0. | | | 0 . | • |
| | | LL. | •• | | 0. | 0, | J. | | • | •0• | • | | • | 0. | | 0 . | 0. | .0 | •0 | | | u. | | | • | | ů. | u. | 281385 +02 | 26849E+02 | 239745+02 | • 8U 1U 4E FU C | . 103335 TUC | | .318625+03 | . 221 × 6E + 0.3 | 14178E+03 | 16.37 DE +0.3 | 628295+62 |
| km | | เม | 0. | •0 | 0. | • 0 | Ū, | 0. | .28435E+00 | •24646E+UV | 0013300000 10130000 | -23267F+01 | .52480E+01 | 31606E+01 | .37548E+01 | •63111E+01 | .11042E+01 | .33351E+01 | .77475E+01 | | | ω | | ••• | • • | • | | 0. | .42287E+02 | •40715E+02 | .44760E+02 | 69518E+U2 | | - 31200503 | 33943F+03 | - 230705403 | -200366+03 | 225895+03 | •10330E+03 |
| AIR AT 60 | | COEFFICIEMTS J | 0. | 0. | 0. | 89034E-01 | 37582E-01 | 14184£*00 | 21193E+00 | 35525E+00 | | 4114957444 | .12877F+01 | .11588E+01 | .11755E+01 | .25501E+01 | 61196E+00 | .12769E+01 | .49248E+0 1 | | COEFFICIENTS | a | | •0• | • | u. 758/15+/// | 35591E+00 | 32784E+00 | .37884E+01 | •36428E+01 | • 39441E+01 | 288836+01 | 28192E+Ul | | 240700ETU2 24026F402 | - 264475402 | -493466+02 | 5 2 05 5F + 1 2 | •31301E+02 |
| LE IN REAL | | Ć FIT | •20671E-03 | .22364E-03 | .21235E-03 | •85084E-02 | .92402E-02 | .13710E-01 | .33371E-01 | .58082E-01 | 10-10000. | •130005400 | - 120175+00 | 163166+03 | 12761E+00 | 344.802+00 | .25821E+00 | 15875E+00 | 909536+00 | | FIT | с | | • 4 52 525-04 | .69348E-04 | | .33016E-01 | .301376-01 | 37538E+00 | 35979E+00 | 38386E+00 | •40225E+00 | | 001301777 • | . 58 34 5 404 | 10.110004 | 43640F+At | - 00537F401 | -,59583E+01 |
| SSION SOURC | | e | 65351E-01 | 66323E-01 | ò3056E-01 | .18032E+00 | .19941E+00 | 30547E+00 | .21518E+00 | •42987E+00 | .58/34E+4U | • > 5 6 8 0 C - U 3 | | 307145401 | 35068F+01 | 65347E+01 | 28099E+00 | 34546E+01 | 97723E+01 | | | ¢ | | 32548E-01 | 36515E-01 | 1973952410 070505400 | .97265E+00 | •90362E+00 | 15385E+02 | - . 14848E+N2 | 16180E+02 | •11959E+02 | .11582E+U2 | - 202070-00 | • 95095492 | • 1 U C U U C T U O | - 108805403 | 207323211 | -************************************* |
| Ъ. Т. | | A | 21878E+02 | 18141E+02 | .30898E+01 | 23467E+02 | 19948E+02 | 22309E+00 | 23627E+02 | 20172E+02 | 22732E+UU | 238662+UC | | | | 149386+01 | 23662E+02 | 20682E+02 | 15379E+01 | | | А | | 22825E+02 | 22795E+02 | - 10110E*02 | 27094E+02 | 58473E+01 | 28258E+02 | 28401E+02 | 71881E+01 | 45556E+02 | 45247E+02 | 13/985+02 | 76525E+U2 | | - + 4 3 0 U 7 E F U 6 | | 391495+01 |
| | | NAX RHOR GN/CN2 | 108.100 | 108.100 | 106.900 | 26.990 | 26.990 | 26.990 | 9.715 | 9.715 | 9.715 | 5•144 5 144 | 507 + C | 50T 00 | | 3-451 | 2 484 | 2.484 | 2.484 | | MAX | RHOR | החל החל | 108.100 | 108.100 | 106.100 | 26.990 | 26.990 | 9.715 | 9.715 | 9.715 | 5.139 | 5,139 | 5.133 | 3.451 | | 164•0 | | c • t o t 2 • \$84 |
| | | HIN RHOR Gh/Ch2 | 56.790 | 56.790 | 56.790 | 2.889 | 2.889 | 2.883 | • 433 | • 433 | .150 | .318 | 010 | 0100 | 0010 780 | . 285 | -287 | .287 | •287 | HMAS | NIN | RHOR | 201 נחל | 5è•790 | 56.790 | 167.94 | 2.889 2.889 | 2.889 | .150 | .150 | .150 | .318 | .318 | .318 | .285 | • • • | 0 0 0 0 0 0 0 | | .287 |
| | NEUTRONS | SAMPLING Altitudé (KM) 00SE | 20.00 SILICON | 20.00 TISSUE | 20.00 FLUENCE | 40.00 SILICON | 46.00 TI. WE | 40.00 FLUENCE | 60.00 SILICON | 60.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 90 00 CI 1720C | | 100011 00 00 + 100 00 | 100.00 FLUENCE | 120,00 STITCON | 120.00 TISSUE | 120.00 FLUENCE | SECONDARY GA | SAMPI ING | ALTITUDE | | 20.00 SILICON | 20.00 TISSUE | 20.00 1 LUENCE | 40.00 SILICON | 40.00 FLUENCE | 60.00 SILICON | 60.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 80.00 TISSUE | 80.CU FLUENCE | 100.00 SILICON | | 140.00 FLUENCE | TLUE OF TANKIN | 120.03 FLUENCE |

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 8

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FIT COEFFICIENTS FOR MORSAIR RUN NO. FISSION SOURCE IN REAL AIR AT 80 km

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.016 .121 .091 .054 .049 .005 RHS PCT DIFF . 762 210 .052 .108 .047 013 RHS PCT DIFF 295 .173 .641 .660 ى . . 23818E+01
23605E+01
45133E+01
45133E+00
43704E+00
43704E+00
43704E+01
55429E+01
55429E+01
17117E+02
17117E+02
182897E+02
982897E+02
10591E+02
10591E+02
10591E+02
10591E+02 34798€+03
36421€+03
36421€+03
263316€+03
580111€+02
580111€+02
53336+02
428596+02
428596+02
428596+02
537906 +03
253336+02
253336+02
10626+04
10626+04
135436+04
135436+04 τu шł COEFFICIENTS D COEFFICIENTS .818855+00 .348945+00 .348945+00 .117635+01 -.75685+01 -.256835+02 -.256835+02 -.256835+02 -.256835+02 -.256835+02 -.256835+02 .149615+03 .149615+03 .153705+03 .153705+03 .153705+03 .153705+03 .299075+02 .299075+02 -.46112E+00 -.46590E+00 -.71227E+00 .50730E+02 .52651E+02 .31608E+02 -.31800E+02 -.25948E+02 .14584E+02 .23897E+03 .256590E+03 .13565E+03 .19160E+04 -.19150E+04 -.38551E+04 -.38551E+04 -.58120E+04 -.55859E+04 -.30771E+04 -.34021E+00 -.20815E+00 -.19058E+00 ٥ FIT FIT 175166 -01
501636 -02
501636 -02
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23452 -04 -.784355-02 -.460945-02 .614915-02 .614915-02 .614601 .253205-01 .253205-01 .253205-01 .343335+01 .343335+01 .343335+02 .149255+02 .343335+02 .149255+02 .149255+02 .148515+02 .148515+02 .148515+02 .197655+02 .197655+02 .197655+02 .19765+02 .19765 .15994E-01 S ω 106246+01 153496+01 -153496+03 -145496+03 -874476+03 -874476+03 -874476+03 -874476+03 -1545456+02 -174286+02 -174286+02 -174286+02 -174286+03 -352106+04 352106+04 -337466+04 -337466+04.916756+00 .522326+00 -726956+00 .627126+00 .3382522400 .3382522400 .336076401 -207536+01 .49834E+01 .68190E+01 .11502E+02 .29818E+01 -.82720E+01 -.19532E+02 -.71950E+02 -.75330E+02 -.33419E+02 -.34633E+02 -.34633E+02 -.34633E+02 -.21340E+01 -.62138E+00 .10532E+01 -.36844E+01 -.19492E+01 œ ത -.51858E+02 -.36148E+02 .23901E+02 -.23769E+02 -.19987E+02 -.26578E+02 -.58976E+01 .58018E+01 .78355E+01 .10065E+02 .38447E+02 -.38447E+02 -.15798E+02 -.15798E+02 -.35344E+02 -.35344E+02 -.34753E+02 -.629?6E+02 -.29660E+92 -.95476E+02 -.928012+02 -.51749E+02 .40026E+02 .15987E+02 -.26538E+02 .34551E+02 --65284E+02 ٩ ٩ 64.860 64.860 12.900 12.900 12.900 12.510 3.404 3.404 HAX KHOR GM/CM2 HAX RHOR GH/CH2 • 153 • 153 .114 .114 .114 64.860 64.860 56.900 56.900 36.900 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.008 3.005 3.0 66.900 36.900 36.900 36.900 3.008 3. HIN RHOR GH/CH2 HIN RHOR Gh/Ch2 015 0150015 15 0 SECONDARY GAHHAS ω in SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICUN TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE SILICON TISSUE SILICON FLUENCE SILICON TISSUE FLUENCE SILICON TISSUE Fluence DOSE DOSE FLUENCE NEUTRONS SAMPLING Altitude (KM) SAMPLING ALTITUDE (KM) 100.00 120.00 120.00 120.00 120.00 140.00 140.00 20.00 20.00 20.00 40.00 80.00 80.00 20.00 20.00 20.00 40.00 40.00 60.00 60.00 80.00 120.00 120.00 140.00 140°00 140°00 40.00 60.00 00.00 80.00 100.00 100.001 140.00 100.00 60.00 40-00 60.00 80.00 80.00 100.001 100.001 120.00

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 10 THERMONUCLEAR SOURCE IN A HOMOGENEOUS ATMOSPHERE

| RHS | DIFF | .831 .884 | .310 | .272 | .308 | .228 | •639 | .671 | | | RHS PCT DIFF | • 395 | • 369 | 312 | .328 | | . 302 | 1 | • 402 | 104. |
|----------------------|-----------------------|--------------|--------------|--------------------------|--------------|--------------------------|--------------|------------------------|--------------|--------------|-----------------------------------|------------------------|---------------|-------------|--------------|------------------------|----------------------------------|--------------------------|------------------|-----------------------------|
| ى | | 0. | •••• | | 0. | ••• | ••• | 0. | • 0 | | ى | 0. | 0. | ••• | • | | ••• | | •0• | ů ů |
| Ľ | | 0. 0. | ••• | •••• | 0. | ••• | 0. 0. | • 0 | ů. | | L. | . | 0. | 0. | • | • • | .22353E+02 | .22351E+U2 .20541E+D2 | 0. | • • • • |
| LU A | 1 | ••• | . | ••• | 8. | 53114C-UL .12794E+00 | .90695E+00 | • • | • • | | ы | 0. | •0 | 0. | • • | • • | 12623E+02 | 12618E+UZ | 0. | 0. |
| COEFFICIENTS D |) | ••• | | 47837E-U2 64761E-U2 | 96085E-02 | 47114E-UC 75568E-O2 | .16031E-02 | 0. | 0. | | r COEFFICIENT: D | 0 . | • | 0. | 11961E-01 | 120/VE-U1 14890F-01 | 37779E-01 | 37208E-01 | -• 3664JC-44 | • • • |
| ر FII | þ | • 0 | | .15232E-03 .19553E-03 | .33873E-03 | .10865E-03 .25930E-03 | .29659E-04 | ••• | 0. | | C FL | c | • | • | •39443E-03 | .40735E-03 | .914302-03 | •89528E-03 | • / 0C42C-03 | °0. |
| ۵ | D | 40110E-01 | 33455E-01 | .43977E-02 | .38390E-01 | .14645E-01 .20062E-01 | 11352E+00 | 40140E-01 | 38262E-01 | | 8 | - 231,21,5 <u>-</u> 01 | | 24603E-01 | •79339E-01 | .78160E-01 | • 10 1 7 05 7 0 0 • 64668E+00 | .64134E+00 | 21935E-01 | 22005E-01 20591E-01 |
| | ч | 20836E+02 | "26092E+01 | 22309E+02 | .15816E+01 | 22338E+02 20209E+02 | 402095+00 | 20935E+U2 17741E+02 | .31649E+01 | | ч | C01300000 | - 014 705 FUC | -67622E+00 | 23328E+02 | 23365E+02 | 36942E+02 | 36954E+02 | 21176E+U2 | 21290E+02 .22201E+00 |
| HAX | KHUK GM/CM2 | 192.600 | 192.600 | 192.900 | 177.500 | 200.000 | 200.000 | 200-000 | 200-000 | | NAX RHOR GN/CM2 | | 192.500 | 192.600 | 192.900 | 192.900 | 192.90U 200.000 | 200.000 | 200.000 | 200.000 |
| NIW | RHOR 6M/CM2 | 101.600 | 101.000 | 21.500 | 21.800 | 3.647 | 8.737 | 101.600 | 101.600 | AHHAS | HIN RHOR GN/CM2 | | 101.600 | 101-600 | 21.800 | 21.800 | 21.800 | .091 | .091. 101.500 | |
| NEUTRONS SAMPLING | ALTITUDE (KM) DOSE | 3.11 SILICON | 3.11 FLUENCE | 3.83 SILICON | 3.83 FIUENCE | 4.01 SILICON | 4.01 FLUENCE | 4.92 SILICON | 4.92 FLUENCE | SECONDARY GI | SAMPLING Altitude (Km) dose | | 3.11 SILICON | 3.11 IISSUE | 3.83 SILICON | 3.83 TISSUE | 3.83 FLUENCE | 4.01 TISSUE | 4.01 FLUENCE | 4.92 TISSUE 4.92 FLUENCE |

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 11 THERMONUCLEAR SOURCE IN REAL AIR AT 20 km

| | RHS PCT DIFF | 1.473 1.548 .729 .729 .224 .265 .393 .265 .393 .265 .415 .392 .392 .392 .392 .392 .392 .395 | RMS PCT DIFF | 425 4235 4235 4235 424 424 424 424 424 424 424 424 424 42 | |
|----------|-----------------------------------|---|-----------------------------------|---|---------------|
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| | S | | S | | • |
| | F COEFFICIENT D | 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | COEFFICIENT D | 6. 10. 10. 10. 10. 10. 10. 10. 10 | 452564-02 |
| | C FI | $\begin{array}{c} 0\\729976-05\\729976-05\\729346-05\\503346-05\\550346-05\\550346-05\\550346-05\\35178-03\\1188266-03\\1188266-03\\1864566-03\\1864566-03\\1864566-03\\1864566-03\\1864566-04\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\1864666-03\\186666-03\\186666-03\\18666666\\18666666\\18666666\\18666666\\18666666\\18666666\\18666666\\18666666\\18666666\\18666666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\1866666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\186666\\18666\\186666\\18666\\18666\\186666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\18666\\1866\\1866\\18666\\1866\\ $ | FIT C | $\begin{array}{c} 0 \\ 0 \\ -22296 \\ -22296 \\ -22379 \\ -20379 \\ -20379 \\ -20379 \\ -20379 \\ -20379 \\ -20379 \\ -104 \\ -105 \\ -103 \\ -47150 \\ -0328 \\ -103 \\ -4128 \\ -103 \\ -4128 \\ -103 \\ -528 \\ -103 \\ -528 \\ -103 \\ -528 \\ -103 \\ -528 \\ -103 \\ -2769 \\ -2769 \\ -2769 \\ -2769 \\ -2769 \\ -2769 \\ -2769 \\ -2769 \\ -2760 \\ -276$ | •16494E-UJ |
| | 8 | -,42995E-01 -,372905E-01 -,359105-01 -,359105-01 -,359105-01 -,359105-01 -,359105-01 -,3504905-01 -,3504905-01 -,503426-01 -,503426-01 -,503426-01 -,503426-01 -,503426-01 -,35546-01 | ß | | .13698E-UI |
| | ব | -20692E+02 18236E+02 18236E+02 21656E+02 21656E+02 219331E+02 219331E+02 217468E+01 21346E+01 21346E+02 19534E+02 21354E+02 210569E+02 210569E+02 21070E+02 21070E+01 28118E+01 | A | -22964E+02 -22556E+02 -225556E+02 -225556E+02 -225556E+02 -22537E+02 -225337E+02 -22337E+02 -223337E+02 -223197E+02 -223197E+02 -223197E+02 -223197E+02 -223197E+02 -223197E+02 -225556+01 -225693E+02 -225695E+02 -225695E+02 -225695E+02 -225695E+02 -225695E+02 -225695E+02 -225695E+02 -2257665E+02 -2257665E+02 -2257665E+02 -2257665E+02 -2257665E+02 -22576655 -22576655 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225766555 -225765555 -225765555 -225765555 -225765555 -2257655555 -2257655555 -2257655555 -22576555555 -225765555555555555555555555555555555555 | 1UJU6E+U1 |
| | MAX RHO' GH/CP | 195.400 200.000 200.000 200.000 195.400 195.400 197.500 197.500 197.500 197.500 197.500 197.500 197.500 197.500 198.400 197.500 198.4000 198.40000 198.40000 198.4000000000000000000000000000000000000 | MAX RHDR GH/CH2 | 195% 400 195% 400 200% 400 200% 400 200% 400 195% 4000 1000000000000000000000000000000000 | 182.700 |
| | HIN RHOR GM/CM2 | 146.500 77.7700 77.77000 77.77000 77.77000 77.77000 77.7700000000 | HIN RHOR GH/CH2 | 146.5000 146.5000 146.5000 146.5000 146.5000 146.5000 146.5000 146.50000 146.5000 146.50000 146.50000 146.5000000000000000000000000000000000000 | 47.91U |
| NEUTRONS | SAMPLING Altitude (kn) dose | 12.09 SILICON 12.09 TISSUE 14.85 SILICON 14.85 FLUENCE 20.61 TISSUE 20.61 TISSUE 20.61 TISSUE 22.08 FLUENCE 22.08 FLUENCE 22.08 FLUENCE 22.08 FLUENCE 22.08 FLUENCE 22.08 FLUENCE 22.13 SILICON 22.13 FLUENCE 24.72 TISSUE 34.72 FLUENCE 34.72 FLUENCE 34.72 FLUENCE 34.72 FLUENCE | SAMPLING Altitude (kh) dose | 12.09 SILICON 12.09 TISSUE 14.85 SILICON 14.85 TISSUE 14.85 TILECON 20.61 TISSUE 20.61 FLUENCE 20.61 FLUENCE 20.61 FLUENCE 22.08 FLUENCE 22.08 TISSUE 22.03 TISSUE 26.13 TISSUE 26.13 FLUENCE 26.13 FLUENCE | 34.72 FLUENUE |
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FIT COEFFICIENTS FOR MORSAIR RUN NO. 12 THERMONUCLEAR SOURCE IN REAL AIR AT 30 km

| | RHS PCT DIFF | 1.218 .934 | • 409 • 75 | | • 430 | • 342 | • 321 | .211 | - 0 - 1 - 0 | 104. | | . 648 | . 602 | - | | RHS | PCT | DIFF | .313 | • 70 • | 0.50 | | • 281 | .300 | .308 | | • 483 | • 475 | | 977 • | • 200 | - 445 - | | |
|----------|-----------------------------------|--------------------------------|--------------------------------|-------------------------------|---------------|---------------|---------------------------|--------------|----------------|-----------------|---------------|-------------------|---------------|---------------|--------------|-------------|----------|----------|---------------|---------------|---------------|---------------|--------------------|----------------------|----------------|---------------|---------------|--------------|---------------|---------------|--------------|---------------|----------------|---------------|
| | J | ••• | | ••• | • | ••• | • • | • | ••• | • | • | • | ••• | • | | | U | | 0. | • • | ••• | • | ••• | • • | • | 0. | .0 | ••• | ••• | . | ••• | • | • | •••• |
| | u. | • • | • • | | • | • | • • | • | • | • | • | • | • | • • | | | u. | | • | • | • | • | • | • • qu.38 7F +0 1 | •10320E+02 | •77550E+01 | • | • | • | • | • | • | • | |
| | ш | | | | 71766E+00 0 | .85378E+00 0 | .locyce+ul U | | | <u></u> | | | | | | | w | | • | | | | . | .87746F+i)1 - | - 10+302.00 | 74814E+01 - | a | | | • | | ⇒ c | | , , |
| | COEFFICIENTS D | | 98193E-02 0 | 412465-U2 U | .81072E-02 | 11293E~01 | .22932E-U1 0.24118E-01 0. | 179796-01 0 | 57490E-02 0. | 14178E-01 0. | .104046-01 0. | 0 Th_3/00TT | 51018F-01 0. | 36145E-01 0 | | OEFFICIENTS | 0 | | | | 0. | 17383E-03 0. | 80026E-03 0. | .3//92E-U2 U. | 491875-01 | 39588E-01 | .30188E-02 0. | 28526E-02 0. | 11528E-01 0. | 19928E-01 0. | 20993E-01 0. | 229836-01 U | | 23913E-01 0. |
| | C FIT (| | 256855-03 | 86811E-04 | 59160E-04 | 21156E-03 | ,58992E-U3 ,10934F-D2 | 895446-03 - | 36654E-03 - | 741576-03 | 462265-03 | | 286535-02 | 16389E-02 | | FIT | c | | • | | | 30690E-04 | 56505E-04 | 15141E-U3 | 121015-02 | 89892E-03 | .30786E-04 | 242936-04 - | 43853E-03 -* | 100596-02 - | 10530E-02 - | 11322E-02 | | 12006E-n2 |
| | æ | .35099E-01 0. .27021E-01 0. | .121726+00 | •6/815E-01 •70954E-01 | .17582E+00 | •19449E+06 | .33091E+00 | .54668E-01 | .20074E-01 | •11752E+00 - | •10309E+00 - | •128/1E+UU | | -25175E+00 - | | | 8 | | .20820E-01 0. | .20719E-01 0. | .22125E-01 0. | .23204E-01 . | .19901E-01 | .96782E-U2 . | . 80 9255 + 00 | 68678E+00 - | .11429E-01 . | .10409E-01 | • 56957E-01 | .84435E-01 | .90950E-01 | .10009E+00 . | •1/200257UU - | .15464E+00 |
| | ٩ | | .1159UE+UI - .20635E+02 - | .13674E+U2 - .29042E+01 - | -23105E+02 - | •-20938E+02 - | .13716E+01 - | •19958E+02 | •14873E+01 - | -21409E+02 - | •18873E+02 - | •222U2E+U1 - | • 201065402 + | •28884E+01 - | | | A | | •22308E+02 - | •22538E+02 - | •16965E+00 - | -22112E+02 - | •22256E+02 - | .11598E+01 | - 23036402 - | -38715E+01 - | •23147E+02 | •23177E+02 | •23491E+01 | •23436E+02 | .23522E+02 | •24581E+01 | - 20157E 4U2 - | •57843E+00 - |
| | MAX RHOR GM/CH2 | - 2000 | L75.000 - | 175.000 - | 200.000 | - 000 - 003 | 168.400 - | L56.000 - | 170.400 | L43.700 - | L36.000 - | [43.700 67 882 | | 19.000 | | MAX | RHOR | GH/CH2 | 192.500 - | - 003.501 | .92.500 - | - 005-861 | 198 . 500 - | 198.500 - | | - 000-002 | 80.000 - | 80.000 - | 90.000 | .43.700 - | - 100.621 | L36.000 - | | - 000°- |
| | HIN RHOR GM/CM2 | 114.200 | 114.200 1 46.240 1 | 46.240 1 46.240 1 | 1.755 | 1.755 2 | 12.200 1 | 11-040 | 11.040 | 13.200 | 13.200 | 13.200 1 | 13.800 1 | 13-800 1 | HNAS | NIN | RHOR | GH/CH2 | 114.200 1 | 114.200 1 | 114.200 1 | 46.240 1 | 46.240] | 46.240 1 | | 1.755 | 11.040 | 11.040 | 14.550 | 13.200 1 | 13.200 1 | 13.200 1 | 13.800 | 17.730 1 |
| NEUTRONS | SAMPLING Altitude (KM) Dose | 15.00 SILICON 15.00 TISSUE | 15.00 FLUENCE 20.00 SILICON | 20.00 TISSUE 20.00 FLUENCE | 30.00 SILICON | 30.00 TISSUE | 30.00 FLUENCE | 40.00 IISSUE | 40.00 FLUENCE | 7 50.00 SILICON | 50.00 TISSUE | 50.00 FLUENCE | 60.00 SILICON | 60.00 FLUENCE | SECONDARY GA | SAMPLING | ALTITUDE | KN) DOSE | 15.00 SILICON | 15.00 TISSUE | 15.00 FLUENCE | 20.00 SILICON | 20.00 TISSUE | 20.00 FLUENCE | 20.00 TISCUE | 30-DO FLUENCE | 40.00 SILICON | 40.00 TISSUE | 40.00 FLUENCE | 50.00 SILICON | 50.00 TISSUE | 50.00 FLUENCE | PU-UU SLLUN | 60.00 FLUENCE |
| | | RHS PCT DIFF | . 461 . 388 | | .153 | • | .108 | * D T • | .108 | •198 | | • 11 • | | .065 | .072 | | | SHS | DIFF | 200 | 715. | | .364 | .366 | .255 | . 250 | | • 355 | • 347 | 231. | | • 723 | .164 | .169 | |
|-------------|----------|-----------------------------------|--------------------------|---------------|-------------------------|---------------|---------------|--------------------------|---------------|--------------|---------------|---------------|--------------|------------------|---------------|----------------|--------------|--------------|----------------|---------|---------------|--------------|---------------|--------------|-----------------|---------------|------------------------|---------------|-------------------------------|---------------|---------------|--------------|---------------|----------------|----------------|
| | | ა | 0. | ••• | 0. 0. | .0 | ••• | ••• | 0. | • | • | u. | • 0 | 0. | . | • 0 | | ¢ | ٥ | | ••• | 0. | •0 | 0. | •0 | | ••• | 0. | ••• | • | • | • | | 0. | 0. |
| | | L. | ů. 0. | | 0. | 0. | ••• | | ů. | | . | • | • | 0. | 0. | 0. | • | ı | Ŀ | | •••• | • • | • 0 | 0. | 0. 20_025402 | - 072055401 | 16227E+02 | 0. | | ••• | • | ••• | ••• | 0. | 0 • |
| 40 km | | w | 0. | 0. | | .0 | 139052+00 | .45923E+UU .15103E+01 | 0. | 0. | • | • | | | .0 | 0. | | ſ | ш | | • • | • | • • | 0. | 0. 116675403 | 2013014774 | .16364E+02 | ŋ. | 0 • | | • | | | • | |
| EAL AIR AT | | COEFFICIENTS D | 0. | •0 | 25323E-01 19933F-01 | 12317E-01 | 21043E-01 | 66707E-02 .30704F-01 | | 16935E-02 | •33652E-02 | •16669E-01 | -+1090E-03 | -71339E-D1 | 55160E-02 | .32076E-01 | | COEFFICIENTS | 0 | | • | • | 28345E-01 | 28232E-01 | 30670E-01 | | .19570E+00 | 11463E+00 | 11513E+00 | 13677E+00 | 75654E-Ul | 77075E-Ul | 81128E-01 | | 75415E-01 |
| SOURCE IN R | | C FII | .15031E-03 .91314E-04 | .735586-04 | •14240E-02 | .74588E-03 | .85599E-03 | •700745-03 | .20131E-03 | 58518E-03 | 20427E-04 | 22222E-02 | • 454 /8E-US | | .55511E-03 | 10934E-02 | | FIT | с | | •35360E-04 | •# 69065=04 | .13331E-02 | .13345E-02 | .14374E-02 | 20-340// 40- | 70956F-02 | .891575-02 | .89397E-02 | •10689E-01 | .64641E-U2 | .65680E-02 | •72226E-02 | 61680F-05 | .78796E-02 |
| MONUCLEAR S | | 8 | 60396E-01 44357E-01 | 38562E-01 | .75666E-01 523575-01 | .174376-01 | .83717E-01 | 86697E-01 | 37580E-02 | 29062E-01 | 11304E+00 | 80960E-01 | 328UZE-UI | 817685-01 | 55237E-01 | 24794E+00 | | | 8 | | 28237E-01 | | 22692E-UI | .13250E+00 | .15409E+00 | | 14565E+U1 21587F+01 | •36260E+00 | 36520E+00 | •42273E+00 | •20011E+00 | •20573E+00 | .19095E+00 | • 141605700 | •133746+00 |
| THER | | A | 21241E+02 189545+02 | .195856+01 | 22307E+02 | •11573E+01 | 22234E+02 | 20453E+02 | 225526+02 | 197116+02 | •12079E+01 | 220596+02 | 19587E+UZ | - 220665402 | 195156+02 | .155156+01 | | | ٩ | | 22171E+02 | 2222UE+U2 | | 24250E+02 | 31934E+01 | 24992E+UZ | 25263E+U2 310605401 | 24440E+02 | 24472E+02 | 35257E+01 | 23866E+02 | 23905E+02 | 27478E+01 | - 22639545406 | 251266+01 |
| | | NAX RHOR GH/CH2 | 179.300 | 179.300 | 115.600 | 120.000 | 76.530 | 76.530 | 42.630 | 42.630 | 42.630 | 32.420 | 32.420 | 0/1•1/0 0/1 | 04.500 | 24.550 | ۴ | MAX | RHDR GHICH2 | | 179.300 | 179.300 | 120.600 | 120.600 | 120.600 | 76.530 | 76.530 76.530 | 42.630 | 42-630 | 42.630 | 32.420 | 32.420 | 32.420 | 24.55U | 24.550 |
| | | NIV RHOR GH/CH2 | 54.830 54.830 | 56.890 | 10.110 | 11.610 | .750 | .750 | 3445 | 3++2 3 | 4.985 | 3.661 | 3.661 | 2•001 2 0 0 1 | 3-674 | 3.674 | HHAS | NIN | RHOR GN/CH2 | 700 /00 | 54.830 | F4.830 | 1000-10 | 10-110 | 11.610 | •750 | • 750 750 | 3.445 | 3+45 | 4.985 | 3.661 | 3.661 | 5.160 | 310°7 | 3.674 |
| | NEUTRONS | SAMPLING Altitude (KM) Dose | 20.00 SILICON | 20.00 FLUENCE | 30.00 SILICON | 30.00 FLUENCE | 40.00 SILICON | 40.00 TISSUE | 40.00 FLUCNUE | 60.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 80.00 TISSUE | 80.00 FLUENGE | 100.00 TISSUE | 100.00 FLUENCE | SECONDARY GA | SAMPLING | ALTITUDE | | 20.00 SILICON | 20.00 TISSUE | ZU.VU FLUENCE | 30.00 TISSUE | 30.00 FLUENCE | 40.00 SILICON | 40.00 TISSUE | 40.00 SILIGON | 60.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 80.00 TISSUE | 80.00 FLUENCE | 100.60 SILICON | 100.00 FLUENCE |

TABLE 19

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 13

TABLE 20

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FIT COEFFICIENTS FOR MORSAIR RUN NO. 14 THERMONUCLEAR SOURCE IN REAL AIR AT 60 km

| t | RNS PCT DIFF | . 849 . 688 | | .145 | .162 | | .048 | .057 | | . 033 | .026 | | • 146 | - 544 | | .030 | .029 | | | | RHS | PCT | DIFF | 464 | | 514. | 240 | | • • • • | | 60n • | • 403 | 010 | 7CD. | 640. | | • 069 | .065 | | .077 | • 078 | | |
|----------|-----------------------------------|-----------------|--------------|---------------|---------------|--------------|------------------|--------------|----------------|---------------|--------------|----------------|-------------|-------------------|------------|---------------------------------------|----------------|---------------|--|--------------|---------------------|----------|-----------------------|-----|---------------|--------------|---------------|---------------|--------------|---------------|------------------|-----------------------------|---------------|--------------|--------------|--------------|------------------|-------------|-----------------------------------|----------------|-----------------|----------------|----------------|
| | ى | • • | | • | .0 | • | | • | •0 | • | • | • | • | • | 0. | 0. | 0. | | | | | ى | | | • | •••• | • | • | | | • 0 | . . | ••• | .0 | ••• | 0. | . | 0. | 0. | 0. | 0. | 0. | |
| | li. | | | | • | | 0. | .0 | .0 | •0 | •0• | 0. | .0 | .0 | •0• | | | | • | × | | Ŀ | | | • | • | ••• | u . | •0• | • | - 1340 8E +0 2 | 12610E+02 | • 38368E +01 | • 26355E+02 | • 31812E+02 | • 15363E+02 | • 54357E+02 | • 54485E+02 | 35 93 9E +0 2 | •13717E+03 | • 16876E+03 | •13818E+03 | |
| | W | • | • | • | | | 10654E+01 (| 53205E+00 | .84360E+00 | .11863E+01 1 | .26271E+01 | .67420E+01 | .34772E+01 | •51165E+01 | .89003E+01 | 27630F401 | - 41108F401 | | ************************************** | | | L | | | • | | • | •0 | 0. | . | •25682E+02 | 24791E+02 | .79415E+01 | 11737E+02 | 17926E+02 | .19808E+01 | 43540E+02 | 43866E+02 | 20243E+02 | 14134E+U3 | 17896E+03 | 14141E+03 | |
| | COEFFICIENTS D | • 0 | • | | 3653AF-01 | | 750266+00 | 70468E+00 | 53998E+00 | .30111E+00 | •57293E+00 | .23037E+01 | .23168E+01 | .26826E+01 | -46636F201 | • • • • • • • • • • • • • • • • • • • | • 107/0C/10/ | 101361007* | •88/3UE+UI | | COPEETCIENTS | | I | | . | • 0 | • | 23689E+00 | 23268E+00 | 26610E+00 | 26826E+01 | .26231E+01 | .14160E+01 | 26455E+01 | .19710E+01 | •44032E+01 | .47928E+00 | •29357E+00 | •45960E+01 | 12552E+02 | 18588E+02 | 12060E+02 | |
| | FIT G | •97844E-04 | | | | | .11838F+00 | -11326E+DD | 10526E+00 | 43473E-01 | 59545E-01 | 31576E+00 | 475366+00 | 47387F+00 | 772366400 | | 0013000770 | | 18317E+U1 | | 517 | | • | | 27690E-03 | .28204E-03 | .14795E-03 | .20442E-01 | 10-342661. | .23313E-01 | 27U14E+00 | 26457E+00 | 12495E+00 | 38341E+00 | 29106E+3 | 613995+00 | 11881E+00 | 84035E-01 | 79199E+00 | .19859E+01 | .30437E+01 | 194896+01 | |
| | ω | 49680E-01 | 43698E-U1 | 20/402-U1 | -+16112E-04 | | .466485405 | .12306E+01 | .34110E+00 | 93205E+00 | 201996+01 | 624346+01 | 42868F+01 | 57270F401 | | 30130430701 | | 46415E+U1 | 15879E+02 | | | C | 3 | | 70486E-01 | 72210E-01 | 47585E-01 | •68621E+00 | .67655E+00 | .76608E+00 | 10630E+02 | 10376E+02 | 58781E+01 | 56010E+01 | 34919E+01 | 11050E+02 | -31458E+01 | .34964E+01 | 73643F+01 | 39546E+02 | -54782E+02 | -38380E+02 | |
| | A | 21896E+02 | 19215E+02 | •11895E+Ul | 221095+02 | **14470E*UC | - 724 20 C + 62 | 200825402 | 353426+00 | 22726402 | 20085F+02 | 192366401 | - 22276F402 | - 24 64 5402 | | T01376902*- | 230bbE+UZ | 21065E+02 | 23554E+01 | | | ~ | £ | | 20669E+02 | 20738E+02 | .13706E+00 | 25177E+02 | 25195E+02 | 42813E+01 | - • 2 8596E + 02 | 28725E+02 | 10789E+02 | 35269E+02 | -+36086E+02 | 13099E+02 | 38210E+02 | 38250E+02 | - 15004F402 | - 44745402 | 529755+02 | 280635+02 | 12.120001+1 |
| | HAX RHOR GH/CH2 | 108.100 | 108.100 | 108.100 | 22.550 | 066• 2 | 0.0+440 0.046 | 3* L 1 | 0,715 | | | | | | | 0.451 | 2.484 | 2.484 | 2.484 | | | XAH | 2HOLAR | | 108.100 | 108.100 | 108.100 | 26.990 | 26.990 | 26.990 | 9.715 | 9.715 | 9.715 | 5.139 | 5.139 | 5.139 | 3.451 | 3.451 | | 101 - C | 2.484 | 2-484 | 101-1 |
| | HIN RHOR GM/CH2 | 062 * 95 | 56.790 | 56.790 | 2.889 | 2.889 | 301 °7 | | 072 | | | | | | • • • | 982. | •287 | .287 | .287 | HHAS | | HIN | CN0/NS | | 56.790 | 56.790 | 56.790 | 2.889 | 2.889 | 3.194 | .150 | .150 | .150 | .318 | .318 | .318 | 286. | 286 | | • • • • • | • L C - | .01. | 103. |
| NEUTRONS | SAMPLING Altitude (KM) Dose | 20.00 SILICON | 20.00 TISSUE | 20.00 FLUENCE | 40.00 SILICON | 40.00 TISSUE | 40.00 FLUENCE | DO DO TICONO | 50 00 51 15305 | 00.00 FLUCACC | 00.00 %TCCUC | 00.000 1 00000 | | CO IUU-UU SILIGUN | | 100.00 FLUENCE | 120.00 SILICON | 120.00 TISSUE | 120.00 FLUENCE | SECONDARY GA | | SAMPLING | ALIAIUUE IKNI DOSF | | 20.01 SILICON | 20.00 TISSUE | 20.00 FLUENCE | AD-DD STLICON | 40-00 TISSUE | 40-00 FLIFNCE | END STLICON | 60.00 TISSUE | 60.00 FLUENCE | NUCLIC NUCLA | An DD TISSUE | ARADA FUENCE | TOTICS OF TOTICS | | 100 00 112000 | JUUAUU TEUERCE | TCU-CU DITICCIE | 174000 FL3500F | ILU-UU FLUENUE |

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TABLE 21 ļ :

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N. S. S.

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Sec. 19

FIT COEFFICIENTS FOR MORSAIR RUN NO. 15 THERMONUCLEAR SOURCE IN REAL AIR AT 80 km

NEUTRONS

| RHS | DIFF | 1.022 | 1 | .185 | 112. | .076 | • 066 | | .035 | •079 | | .016 | .037 | | .00. | -017 | | • 008 | .009 | • | | | RHS | PCT | DIFF | .427 | +6+• | | • 346 | .348 | | •137 | .133 | | non• | FCU • | 000 | | • "7" | 050 | 200. | +00. | 2002 | 300 | > > > |
|--------------|-----------------------|--------------------------|---------------|---------------|-------------------------|---------------|--------------|---------------|-------------------------------|--------------|---------------|----------------|-------------------------------|----------------|-----------------------------|---------------|-----------------------------|---|--------------|----------------|---|---------------|--------------|----------|-----------|---------------|--------------|-----------------------------|---------------|-------------------------------|-------------------------------|-------------------------------|--------------|-----------------|---------------|--------------|---------------|----------------------------|---------------|----------------|---------------|---------------------------------------|---------------------------|----------------|--------------------------|
| ų | 2 | 0. | ••• | 0 • | • | | 0. | 0. | 0. | 0. | 0. | .0 | 0. | 0. | .0 | 0. | 0. | 0. | 0. | .0 | | | | ß | | 0. | .0 | .0 | 0. | | •• | •0 | ••• | • | • • | • | • | • | • | • | ••• | • | | • | • • |
| ι | L | 0. 0. | 0. | ••• | • | ••• | 0. | 0. | 0. | ••• | 0. | | 0. | 0. | 0. | 0. | .0 | .0 | 0. | | 5 | | | L. | | 0. | .0 | 0. | 0. | 0. | 0. | • 10329E+03 | • 93335E+02 | • IIU/85 +U3 | /4238E +U I | | • 4410/E+02 | • 09/0/070/ / 0320/ 000 | | • 330035 40 5 | | • 333605 TUS | .14183F +04 | • 14TOSC 404 | •126545+04 |
| u A | ц | •0 | | | • | 50377E+01 | 96914E+00 | .46871E+01 | •51343E+00 | 38737E+00 | 75283E+00 | 11057E+01 | .19102E+01 | .93904E+01 | .16410E+01 | .11212E+02 | 22984E+02 | .90426E+00 | .757A7F+01 | 25308E+02 | | | | щ | | 0. | .0 | 0. | 0. | 0. | 0. | 10364E+03 | 92043E+02 | 110406+05 | • > 626/E+UZ | • >6/8UE+UZ | 325785442 | +• 556 500 FUC | 432020402 | -•915446704 | -+0U211CTU3 | 07340E+03 | 76159F+A4 | | 232795+04 |
| COEFFICIENTS | 3 | • | .0 | 14349E+00 | 13954E+UU 22820F400 | 508976+01 | 23877E+01 | •61945E+00 | 11795E+01 | 93475E+01 | 24948E402 | 35520E+02 | 35283E+02 | 14167E+02 | 28172E+02 | •66353E+02 | •136456+03 | 417096+02 | .752A9E+01 | 21346E+03 | | | COEFFICIENTS | 0 | | 0. | •0 | 0. | 45729E+00 | 43680E+00 | 53551E+00 | 12401E+02 | 10799E+02 | 126/1E+UC | • 80890E+02 | -8035/E+UZ | • 49568E+U1 | •22/2UE+U3 | •2062UE+03 | | | /2020E+U3 | | - 643400 ETU4 | -*57965E+04 |
| EII E | C | 32059E-02 | 21110E-02 | .18209E-01 | •1/602E-01 | .11156E+01 | •56572E+00 | •48434E-01 | 93985E+00 | •43925E+01 | .13115E+02 | •2 97 07E +02 | 33683E+02 | •29885E+02 | 37755E+02 | 40514E+02 | +.65230E+02 | -50700E+02 | -18617F+02 | 13722E+03 | | | FIT | o | | 42259E-02 | 72011E-02 | .60706E-02 | .51747E-01 | •49084E-01 | •62410E-01 | 22523E+01 | •19945E+01 | •231//E+U1 | 26385E+UZ | 260765+02 | .4282UE+UU | ••102/4E+00 | 1243UE+US | 2042647740- | • 51581E7US | • • • • • • • • • • • • • • • • • • • | • 4 1 2 1 4 C 4 0 4 | +0.10010000 | .404335744 .42308E+04 |
| ŝ | æ | .36483E+00 .28102E-01 | .17868E+00 | .25390E+00 | .23108E+00 E23E2E+00 | .79842E+01 | -29896E+01 | 34827E+01 | 66020E+00 | • 55613E+01 | .12961E+02 | .13079E+02 | .727316+01 | 15078E+02 | .31382E+01 | 420395+02 | 90866E+02 | .77458F+01 | 21028E+02 | | | | | 8 | | .50399E+C0 | .86602E+00 | 75425E+00 | 10285E+01 | 98591E+00 | 11894E+01 | 。31996E+02 | •27626E+02 | • 330 / UE + UZ | | 95895E+02 | 15262E+U2 | IZ48ZE+U3 | ILL/9E+US | | • 6U185E+U3 | • 04411E+U3 | • 164045704 6.07625406 | +0/2/2/1+0+ | .36165E+04 |
| | 4 | 34946E+02 | 36652E+01 | 22578E+02 | 20025E+02 | 21248E+02 | 20089E+02 | 14060E+01 | 22439E+02 | 20183E+02 | 65852E-01 | 22365E+02 | 20400E+02 | 81041E+00 | 225445+02 | 20902E+02 | 14574E+01 | 22477E+02 | | 13697E+01 | | | | A | | 39011E+02 | 50159E+02 | 21116E+02 | 24993E+02 | 24972E+02 | 41507E+01 | 45474E+02 | 44115E+02 | 26118E+UZ | S1936E+02 | 31900E+UZ | 15214E+U2 | 304/0E+UC | 36/U5E+U2 | 1/149E4U2 | 5362954UC | 542U/E4U2 | | | 75309E+02 |
| MAK | KHOK GM/CM2 | 64.860 64.860 | 63.500 | 12.900 | 12.900 | 3.404 | 3.404 | 3.404 | • 832 | . 832 | . 832 | • 289 | .289 | • 226 | .153 | .153 | .153 | 114 | | | | | MAX | RHOR | GN/CN2 | 64-860 | 64.860 | 64.860 | 12.900 | 12.900 | 12.900 | 3.40% | 3.404 | ショナ・ワ | .832 | . 832 | .832 | - 285 • | • 285 | 582. | •12. | 5 C T T | 70 7 • | • • • | • 11 • |
| NIN | KHUK GN/CN2 | 56.900 56.900 | 56.990 | 3.008 | 3.008 | 2000 | .267 | .267 | .100 | .020 | .020 | .026 | .026 | .015 | .015 | .015 | .015 | .115 | . 015 | .015 | 1 | IHAS | MIN | RHOR | GH/CH2 | 56.900 | 56.900 | 56.900 | 3.008 | 3.008 | 3,008 | .267 | .267 | .267 | .020 | .50. | • 0 2 0 | 6 T D • | eru. | 5TD. | 4TN. | 6110 . | | | .015 |
| SAMPLING | ALTITUDE (KH) DOSE | 20.00 SILICON | 20.00 FLUENCE | 40.00 SILICON | 40.00 TISSUE | AUAUU FLUENCE | 60.00 TISSUE | 60.00 FLUENCE | 80.00 SILICON | 80.00 TISSUE | 80.00 FLUENCE | 100.00 SILICON | 100.00 TISSUE | 100.00 FLUENCE | 120.00 SILICON | 120.00 TISSUE | 120.00 FLUENCE | I T T T T T T T T T T T T T T T T T T T | TTO DU TTOUT | 140.00 FLUENCE | | SECONDARY GAN | SAMPLING | ALTITUDE | (KH) DOSE | 20.00 SILICON | 20.00 TISSUE | 20.00 FLUENCE | 40.00 SILICON | 40.00 TISSUE | 40.00 FLUENCE | 60.00 SILICON | 60.00 TISSUE | 60+00 FLUENCE | BU-UU SILLCUN | su.uu IISSUE | 80.00 FLUENCE | TUU STLLEUN | TUU-UU ILSSUE | IUU.UU FLUENCE | ICO DO ITANON | 120 00 EL VENCE | 120 00 CT 170N | Itue on thread | 140.00 FLUENCE |

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APPENDIX C

MORSAIR SILICON DOSES AND K-FACTORS

For each of the 15 MORSAIR runs, this appendix contains the computer plotted results of:

- 1. The fit of the MORSAIR $4\pi R^2$ silicon dose versus the mass range ("RHOR" in the figures). The different point symbols were calculated from the fits to the MORSAIR data, and the solid line is the fit of the one-dimensional ANISN data.
- The silicon dose K-factors as a function of mass range at each sampling altitude.

In order to reduce the number of plots, several sampling altitudes have been combined on a single figure.





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FIGURE 0-15 MORSAIN FIT DATA-4PIR##2 GAMMA SI DOSE, FISSION SOURCE IN REAL AIR AT 15.0 KM. ALL SAMPLING ALTITUDES

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FISSION SOURCE IN REAL AIR AT 30.0 KM. All JAMPLING ALTITUDES



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FIGURE 0-23 MORSAIN FIT DATA-SPIR**2 GAMMA SI DOSE, FISSION SOURCE IN REAL AIR AT 30.0 KM. ALL SAMPLING ALTITUDES



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FIGURE 3-27 MORSAIN FIT DATA-4PIR##2 GAMMA SI DOSE. FISSION SOURCE IN REAL AIR AT 40.0 KM. ALL SAMPLING ALTITUDES

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FIGURE C+29 MORSAIK FIT DATA-4PIR**2 NEUTRON SI DOSE, FISSION SOURCE IN REAL AIR AT 60.0 KM. SAMPLING ALTITUDES 20 AND 40 KM.



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FIGURE 2-31 FORSAIR FIF DATA-4PIR**2 GAMMA SI DOSE. FIJSION SOURCE IN REAL AIR AT 60.0 KM. SAMPLING ALTITUDES 20 AND 43 KM.



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SAMPLING ALTITUDES 00,80,100, AND 120 KM.



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FISSION SOURCE IN REAL AIR AT 80.0 KM. Sampling Altitudes 20 kilometers.



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> > SAMPLING ALTITUDES 20 KILOMETERS.





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FIGURE 0-43 MORSAIR FIT DATA-4PIR**2 GAMMA SI DOSE. FISSION SOURCE IN REAL AIR AT 80.0 KM. GAMPLING ALTITUDES 40 AND 60 KM.



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SAMPLING ALTITUDES 80,100,120, AND 140 KM.



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FIGURE 3+53 MORSAIN FIT UATA-4PIR**2 NEUTRON SI UOSE, THERMONUCL SOURCE IN REAL AIR AT 20.0 KM. ALL GAMPLING ALTITIDES





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C-65 MORSAIR FIT DATA-4PIR**2 NEUTRON SI DOJE, THERMONUCL SOURCE IN REAL AIR AT 60.0 KM. SAMPLING ALTITUDES 20 AND 40 KM.

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> THERMUNUCL SOURCE IN REAL AIR AT 60.0 KM. Sampling Altitudes 20 and 40 km.

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FIGURE C-71 MORSAIK FIT DATA-4PIR##2 GAMMA SI DOSE, THERMONUCL SOURCE IN REAL AIR AT 60.0 KM. SAMPLING ALTITUDES 50,80,100, AND 120 KM.



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THERMONUGL SOURCE IN REAL AIR AT 60.0 KM. SAMPLING ALTITUDES 60,80,100, AND 120 KM.



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SAMPLING ALTITUDES 20 KILOMETERS.

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GURE C-77 MORSAIR FIT DATA-4PIR+2 NEUTRON SI DUSE. THERMONUCL SOURCE IN REAL AIR AT 80.0 KM. SAMPLING ALTITUDES 40 AND 60 KM.

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SAMPLING ALTITUDES 80,100,120, AND 140 KM.



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